

SHAGRIN FALLS - CAMBRIDGE CTR. R.R.

CAMBRIDGE TWP., WEAUGA CO., O.

80

LEVEL BOOK

744

PLEASE RETURN TO
 GEAUGA COUNTY ENGINEER

TABLE FOR REDUCING PERCHES TO FEET AND INCHES.

PERCH	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.
1	16 6 in.	21	3 46 6 in.	41	6 76 6 in	61	10 06 6 in.	81	13 36 6				
2	33 0	22	3 63 0	42	6 93 9	62	10 23 0	82	13 54 0				
3	49 6	23	3 79 6	43	7 09 6	63	10 39 6	83	13 90 6				
4	66 0	24	3 96 0	44	7 26 0	64	10 56 0	84	14 06 6				
5	82 6	25	4 12 6	45	7 42 6	65	10 72 6	85	14 23 0				
6	99 0	26	4 29 0	46	7 59 0	66	10 89 0	86	14 39 6				
7	1 15 6	27	4 45 6	47	7 75 6	67	11 05 6	87	14 56 0				
8	1 32 0	28	4 62 0	48	7 92 0	68	11 22 0	88	15 12 6				
9	1 48 6	29	4 78 6	49	8 08 6	69	11 38 6	89	15 29 0				
10	1 65 0	30	4 95 0	50	8 25 0	70	11 55 0	90	15 45 6				
11	1 81 6	31	5 11 6	51	8 41 6	71	11 71 6	91	16 02 0				
12	1 98 0	32	5 28 0	52	8 58 0	72	11 88 0	92	16 18 6				
13	2 14 6	33	5 44 6	53	8 74 6	73	12 04 6	93	16 35 0				
14	2 31 0	34	5 61 0	54	8 91 0	74	12 21 0	94	16 51 6				
15	2 47 6	35	5 77 6	55	9 07 6	75	12 37 6	95	17 08 0				
16	2 64 0	36	5 94 0	56	9 24 0	76	12 54 0	96	17 24 6				
17	2 80 6	37	6 10 6	57	9 40 6	77	12 70 6	97	17 41 0				
18	2 97 0	38	6 27 0	58	9 57 0	78	12 87 0	98	17 57 6				
19	3 13 6	39	6 43 6	59	9 73 6	79	13 03 6	99	18 14 0				
20	3 30 0	40	6 60 0	60	9 90 0	80	13 20 0	100	18 30 6				

COURT HOUSE
 CHARDON, O.
 PHONE 250-X

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
 DRAWING MATERIALS AND SURVEYING INSTRUMENTS

BAINBRIDGE CENTER-CHAGRIN FALLS
 ROAD C.H. #9
 BAINBRIDGE TWP. GEAUGA CO., O.,

L. J. McNAUGHTON
 County Engineer

1919

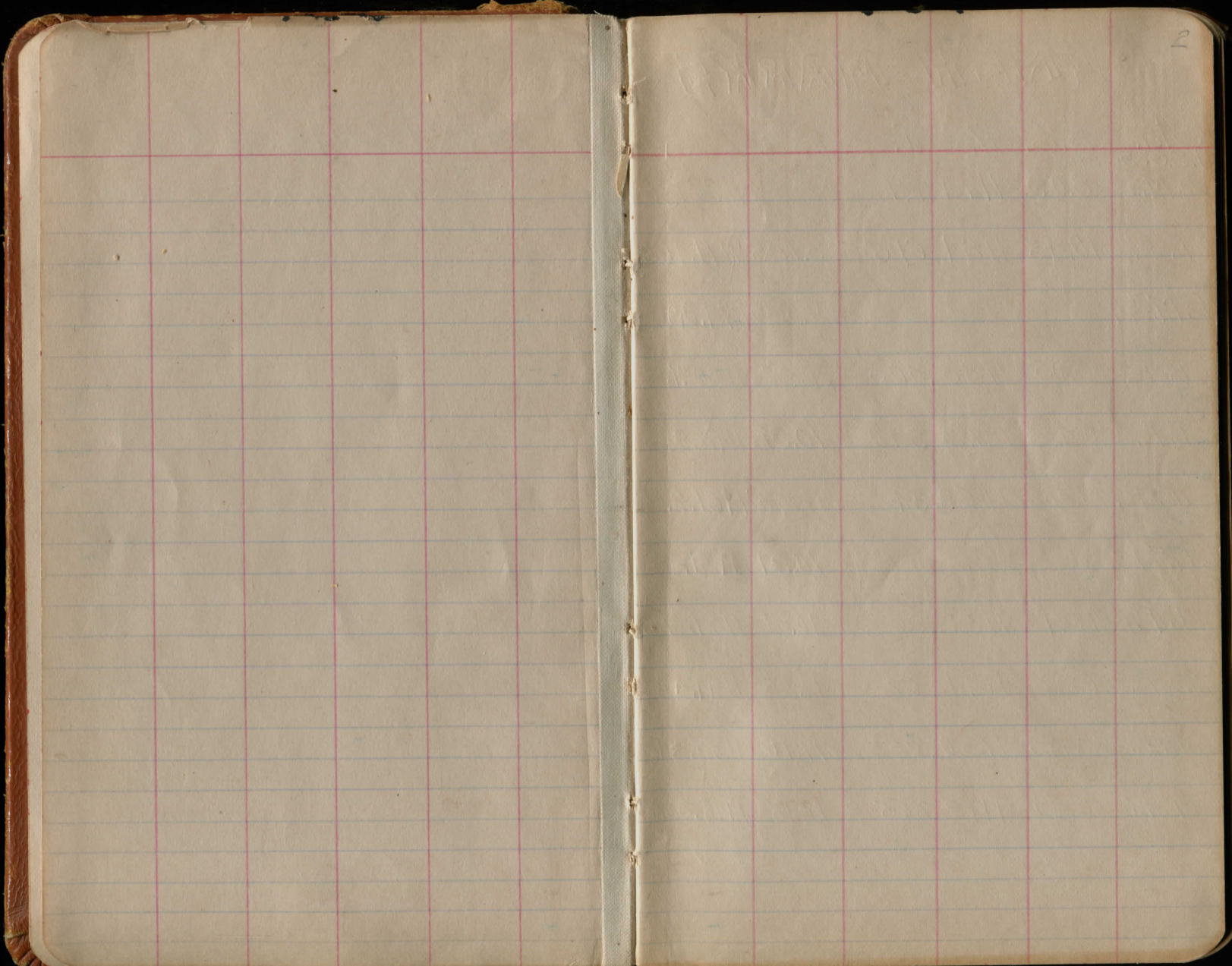
Index on Next Page

80

44
 9 4 8
 0 4 4
 99
 0 1 1
 99
 10 1 1
 0 6 6 99

1919 INDEX 1919

Bench Marks 3-8
X Sections & Drainage 10-44



BENCH MARKS

10-10-19
Temp. Windy.
Hot.
Rain.

Harold
Thompson

3

Sta. B.S. H. I. F.S. Elev.

U.S.G.S.

B.M. 8.09 1174.27 1166.180 Aluminum Tablet N. parapet.

T.P. 10.45 1181.615 3.105 1171.165

B.M.#14 7.525 1174.09 On 3' Elm 25' Lt. Sta. 179+20

T.P. 3.05 1183.805 0.86 1180.755

T.P. 0.455 1173.340 10.92 1172.835

T.P. 1.08 1162.34 12.08 1161.26

B.M.#13 10.91 1151.43 On 5' root 18" Bitter Nut 40' Lt. Sta 155+50

T.P. 1.51 1152.96 10.89 1151.45

T.P. 0.21 1141.62 11.55 1141.41

T.P. 0.475 1130.985 11.11 1130.51

T.P. 0.43 1119.265 12.15 1118.835

✓

H. I.
Sta. B.S. 1119.265 F.S. Elev.

T.P. 0.115 1107.910 11.47 1107.795

B.M.#12 1.39 1106.52 On M.W. root 18" Elev, 23" Pt. Sta 1199.68

T.P. 0.06 1095.86 12.11 1095.80

T.P. 0.06 1084.45 11.47 1084.39

T.P. 0.19 1072.575 12.065 1072.385

T.P. 0.185 1060.520 12.24 1060.335

T.P. 0.61 1049.33 11.80 1048.72

B.M.#11 4.72 1044.61 On N. root 18" Evergreen in door yard 40' r.H. Sta. 139+75

T.P. 0.41 1037.99 11.75 1037.58

T.P. 0.68 1027.12 11.55 1026.94

T.P. 2.82 1018.05 11.89 1015.23

✓

H. I.

Sta	B.S.	1018 05	F.S.	Elev.	
B.M.#10			6.35	1011.70	On N.E. root 40" Elm 22' ft., Sta. 130+50

T.P.	9.79	1026 76	1.08	1016.97	Field N.E. wing.
------	------	---------	------	---------	------------------

T.P.	11.85	1038 56	0.03	1026.73	
------	-------	---------	------	---------	--

T.P.	12.13	1050 15	0.54	1038.32	
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T.P.	12.02	1062 06	0.11	1052 04	
------	-------	---------	------	---------	--

T.P.	11.34	1073 09	0.31	1061.75	
------	-------	---------	------	---------	--

B.M.#9			0.58	1072.51	On N.E. root 12" Maple, 25' ft. Sta. 121+25
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T.P.	10.70	1083 17	0.62	1072.47	
------	-------	---------	------	---------	--

T.P.	11.095	1093 905	0.36	1082.31	
------	--------	----------	------	---------	--

T.P.	11.145	1104 22	0.83	1093.075	
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T.P.	9.02	1112 955	0.285	1103.936	
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✓

H. I.

Sta. B.S. 1112 955 F.S. Elev.

B.M.#8 4.74 1103.215 On N.E. root end maple, 23' Pt. Sta. 114+35

T.P. 10.635 1123.020 0.57 1112.385

10-12-10
Fair-Cold

T.P. 5.51 1126.425 2.105 1120.915

T.P. 11.26 1135.90 1.785 1124.640

T.P. 5.72 1141.25 0.37 1135.53

B.M.#7 3.91 1137.34 On N.E. root 20" Maple, 35' Pt., Sta. 97+40

T.P. 0.21 1131.055 10.405 1130.845

T.P. 0.305 1119.325 12.035 1119.02

T.P. 4.30 1117.38 6.245 1113.033

B.M.#6 5.94 1111.44 Nail in N.E. root 30" Maple, 35' Pt., Sta. 72+15

T.P. 1.80 1108.28 10.90 1106.48

1108.22	1115.30 HI	1177.6
7.08	1.08	1174
1115.30	1114.22 -	
1108.22	10.37	
5.50	1124.58	720
	1117.40	470
	7.28	250
1115.30		
1109.5		
5.80		

c 4.5 c 2.5

✓

Sta. B.S. H. I. F.S. Elev.

T.P. 2.04 1100 22 10.10 1098.18

B.M.#5 3.62 1096.60 On N. root 36" Maple, 40' Ft. Sta. 62+45.

T.P. 0.295 1090 01 10.15 1089.805

T.P. 2.71 1080 95 11.77 1078.24

T.P. 1.03 1070 25 11.73 1069.22

T.P. 1.38 1060 405 11.225 1059.625

B.M.#4 6.655 1053.75 On N.W. root Twist Elm, 25' Ft., Sta. 43+10

T.P. 0.805 1049.28 11.93 1048.475

T.P. 1.32 1040 55 10.05 1038.23

T.P. 0.58 1029 705 11.425 1029.125

T.P. 0.685 1018 545 11.845 1017.860

✓

Sta B.S. H. I. F.S. Elev.
1018.545

T.P. 1.445 1010 16 9.83 1008.715

B.M.#3 4.38 1005.78

On N. foot 24" Elev, 28' Rt., Sta. 20+50

T.P. 0.285 999.015 11.43 998.73

T.P. 0.31 987.705 11.62 987.395

T.P. 0.035 976 105 11.635 976.07

T.P. 0.525 964.56 12.07 964.035

B.M.#2 6.52 958.04

x on W. end N. Head wall to Drive Rt.

T.P. 0.58 953 95 11.19 953.37

T.P. 0.235 942.535 11.55 942.40

3.74 938.795

¢ pavement at end Co. line.

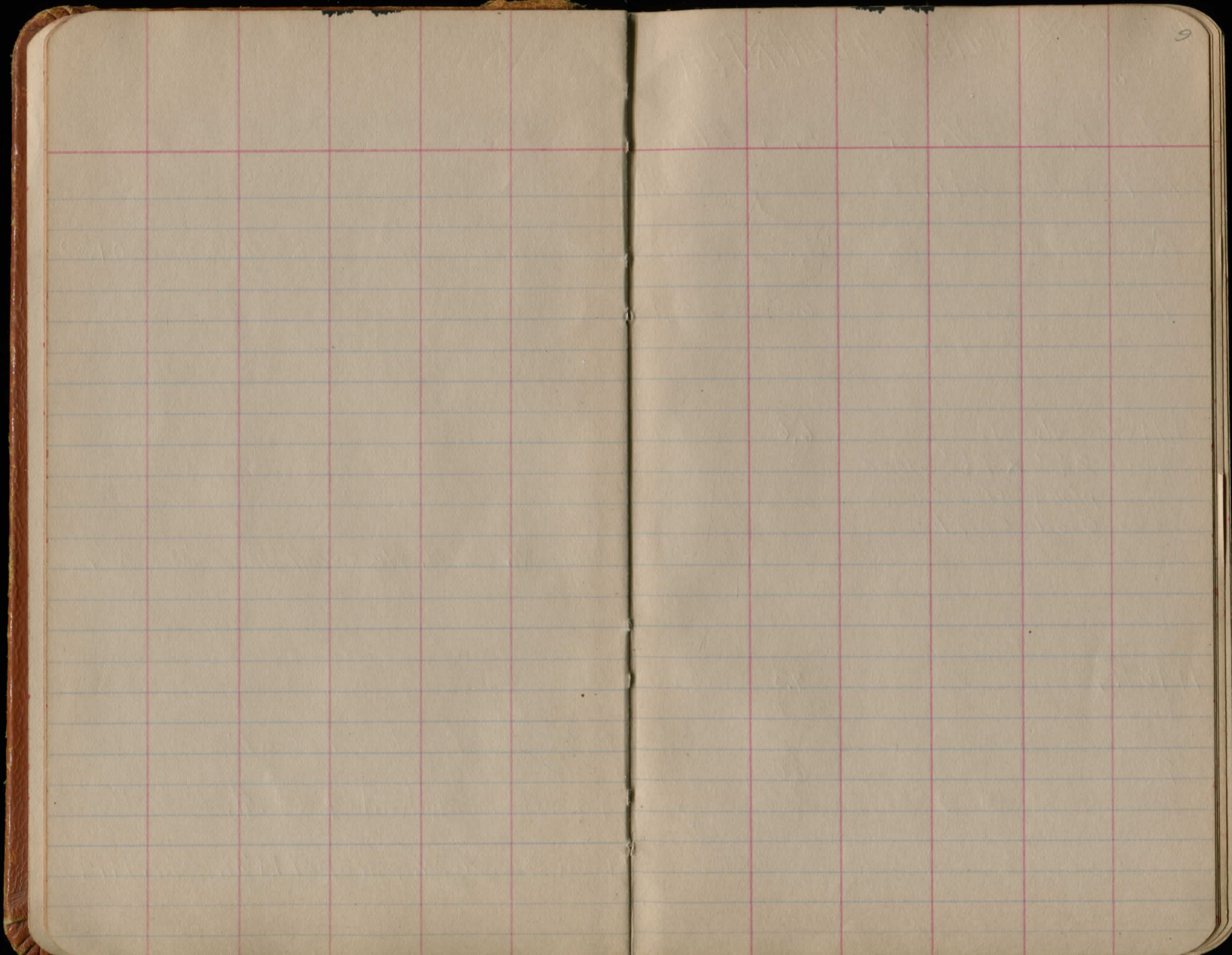
6.215

Top of monument ¢ of St. 6' E. of curb

B.M.#1 9.265 933.27

x on S. end W. parapet 24' Rt. Sta. 1+14





10-23-19

Drake
Hart 79.

X SECTIONS

10

Sta. B.S. H. I. F.S. Elev

B.M.#1 8.02 941.29 932.29 x on S. end W. parapet.

0 2.5 38.8 \ominus end of pavement

1 6.9 34.4

-0.9	-1.9	-0.5	+0.1	0.0	0.0	-1.1	-3.8
<u>7.8</u>	<u>8.8</u>	<u>7.1</u>	<u>6.8</u>	<u>6.9</u>	<u>6.2</u>	<u>8.0</u>	<u>10.7</u>
25-21	17	8	3		9	14	25

+14 \ominus Culvert. 6.6 34.72½' x 2½' Stone
plank floor
Good Condstone conduit 16'-4" x 23'-6"
from under
right
3' opening
for ditch water

-5.6	-0.1	-1.5	0.0	-2.2	-1.4	-5.7
<u>12.2</u>	<u>6.7</u>	<u>8.1</u>	<u>6.6</u>	<u>8.8</u>	<u>8.0</u>	<u>12.5</u>
14.8	16	14	00	22	23	29
FL1						FL1

+40 P.C. 7.3 34.0

-2.4	-1.9	+0.1	0.0	-0.2	-0.7	-4.2
<u>9.7</u>	<u>9.2</u>	<u>7.2</u>	<u>7.3</u>	<u>7.5</u>	<u>8.0</u>	<u>11.5</u>
25	19	6		11	16	25

2 6.0 35.3

-2.0	-2.7	-2.0	-0.3	0.0	+0.5	-0.1	-1.0
<u>8.0</u>	<u>8.9</u>	<u>8.0</u>	<u>6.3</u>	<u>6.0</u>	<u>5.5</u>	<u>6.1</u>	<u>7.0</u>
25	16	8	1		11	25	3.5 edge of sill

H. I.
Sta. B.S. 941 29 F.S. Elev
3 2.5 38.8
T.P. 11.19 951 01 1.47 939.82

3+63.4 16" Iron pipe 11.1 39.9

4 10.8 40.2

+50 8.6 42.4

5 6.2 44.8

6 2.1 48.9

T.P. 10.76 960.51 1.26 949.75

Under RR Bridge

-0.5	0.0	-1.0	-0.5
<u>3.0</u>	2.5	<u>3.5</u>	<u>3.0</u>
11		10	11

← 19' → 19'

-2.8	-0.4	+0.2	0.0	-0.4	-1.7	-1.3
<u>13.2</u>	<u>12.5</u>	<u>10.5</u>	<u>11.1</u>	<u>11.5</u>	<u>12.8</u>	<u>12.4</u>
20	19	12	00	9	10	18

FL

-2.5	0.0	+0.2	0.0	-0.2	-1.2
<u>13.3</u>	<u>12.8</u>	<u>9.9</u>	<u>10.8</u>	<u>11.0</u>	<u>12.0</u>
25	17	9	16	8	25

FL

-2.0	-1.8	-0.3	0.0	+0.1	-0.6	-2.7
<u>10.6</u>	<u>10.7</u>	<u>8.5</u>	<u>8.6</u>	<u>9.0</u>	<u>9.6</u>	<u>11.2</u>
26	13	9	8	6	11	16-25

-1.6	-1.5	-0.2	0.0	-0.1	-1.8	-2.2
<u>8.8</u>	<u>7.7</u>	<u>6.4</u>	<u>6.2</u>	<u>6.3</u>	<u>8.0</u>	<u>8.4</u>
25	12	8	00	9	14	25

+4.3	+1.1	+0.5	-0.2	-0.1	0.0	-0.3	-1.5	-0.6	+0.3
<u>22.10</u>	<u>16.2</u>	<u>2.3</u>	<u>2.2</u>	<u>2.1</u>	<u>2.4</u>	<u>3.6</u>	<u>2.7</u>	<u>2.4</u>	<u>2.4</u>
25	20	16	13	7	9	14	18	18	25

✓

Sta. B.S. H. I. F.S. Elev.
 6+34.99 960 51 10.4 50.1

7- 7.6 52.9

7+54 ♀ stone Culv.
 3' x 3 1/2' box
 No flood
 Good cond

5.5 55.0

B.M.#2

2.77 ^{558.04} 958.04

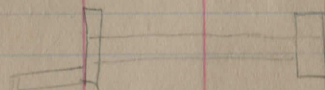
8 4.0 56.5

T.P. 11.12 969 16 958.94

9 8.1 61.1 ✓

+5.5 +1.5 +0.1 +0.2 0.0 -0.1 -1.8 -0.3 -0.5
~~3.2 8.9 10.3 10.2 10.4 10.5 12.7 10.7 10.9~~
 25 18 13 9 8 10 18 25

+2.7 +0.8 +0.4 0.0 -0.1 -1.5 -3.6
 1.9 6.8 7.2 7.6 7.7 9.1 11.3
 25 14 5 10 16 25



x 12'-6" x 13
 -6.0 +0.3 -0.4 -0.5 0.0 +0.2 +0.5 -0.2
 1.3 5.1 5.9 6.0 5.5 5.3 5.0 11.7
 13 12 11 5 20 11 13 14
 FL RL

x 50' w. end N. Head-wall Culv. on drive to Rt.

-2.3 -1.0 -0.6 0.0 +0.2 -0.5 -2.6 -0.4 -0.2
 6.3 5.0 4.6 4.0 3.8 4.5 6.6 4.4 4.6
 25 13 6 8 12 16 19 25

-1.4 -0.6 -0.7 -1.5 -0.5 0.0 +0.1 -1.3 -2.0 -0.7 +0.7
 9.7 9.7 8.8 9.6 8.6 8.1 8.0 9.4 10.1 8.8 7.2
 25 16 8 4 5 9 12 14-16 19 25

H J
Sta B.S 969 16 F.S. Elev
9425 P.C. 6.4 62.8

10 1A 67.8

T.P. 11.30 979⁸ 7.8 0.68 98.18

PT. 5000
11 52 74.6

T.P. 12.23 991 9.2 0.09 99.09

12 11.7 80.7

13 7.1 84.8

14 3.1 88.8

T.P. 11.83 1002 17 1.58 89.13

-0.5 -0.7 -0.4 -1.4 -0.4 0.0 +0.2 -0.8 -1.8 -0.3 +2.3
 $\frac{6.9}{2.5} \frac{7.1}{1.5} \frac{6.8}{10} \frac{7.8}{7} \frac{6.3}{5} \frac{6.4}{8} \frac{6.2}{11} \frac{7.2}{15} \frac{8.2}{16} \frac{6.7}{21} \frac{4.1}{25}$

+2.4 -0.4 -1.0 -0.4 -0.6 0.0 +0.7 -0.8 +5.2 +5.4
 $\frac{-1.0}{2.5} \frac{1.2}{1.8} \frac{2.4}{16} \frac{1.8}{8} \frac{2.0}{6} \frac{1.4}{11} \frac{0.7}{11} \frac{2.2}{14} \frac{-3.8}{22} \frac{-4.0}{25}$

+6.2 +2.6 -1.2 -3.3 -0.7 0.0 -0.2 +0.2 -0.4 +0.9 +4.0 +4.7
 $\frac{-1.0}{2.5} \frac{2.6}{1.9} \frac{6.4}{13} \frac{8.5}{11} \frac{5.9}{7} \frac{0.2}{4} \frac{5.4}{9} \frac{5.0}{12} \frac{5.6}{15} \frac{4.3}{16} \frac{1.2}{20} \frac{0.6}{25}$

+3.7
 $\frac{8.0}{1.1} \frac{-0.5}{1.1} \frac{-1.3}{1.1} \frac{-0.4}{1.1} \frac{-0.6}{1.1} \frac{0.0}{1.1} \frac{-0.2}{1.1} \frac{-0.9}{1.1} \frac{+0.1}{1.1} \frac{+2.2}{1.1} \frac{+2.7}{1.1}$
 $\frac{+1.5}{1.1} \frac{1.0}{1.1} \frac{1.2}{1.1} \frac{1.3}{1.1} \frac{1.2}{1.1} \frac{1.7}{1.1} \frac{1.3}{1.1} \frac{1.2}{1.1} \frac{1.6}{1.1} \frac{1.6}{1.1} \frac{2.5}{1.1} \frac{2.0}{1.1}$

+2.9 +0.6 -0.8 -1.4 -0.8 -0.6 0.0 -0.1 -1.3 +0.6 +1.1
 $\frac{4.2}{2.5} \frac{6.5}{1.8} \frac{5.7}{1.4} \frac{3.3}{1.2} \frac{7.5}{9} \frac{7.1}{4} \frac{7.1}{1.2} \frac{7.2}{1.4} \frac{8.1}{1.5} \frac{6.5}{1.8} \frac{6.9}{2.5}$

+4.3 +2.3 -1.1 -0.7 0.0 +0.1 +0.4 -0.7 +4.5 +1.7
 $\frac{-1.2}{2.5} \frac{0.8}{2.2} \frac{4.2}{1.9} \frac{3.8}{1.3} \frac{3.1}{4} \frac{3.0}{8} \frac{2.7}{1.2} \frac{3.8}{1.4} \frac{1.6}{1.5} \frac{1.6}{2.0} \frac{1.4}{2.5}$

✓

Sta B.S. 1002² 17 F.S. Elev
 15 9.3 92.9

16 6.6 95.6

15+91 @ 12" #1P 6.9 95.3

10-21-19
 cold-cloudy

T.P. 11.52 1006¹ 56 7.30 994.84

17 8.6 97.8

18 6.9 99.5

19 5.6 100.8

20 7.1 102.3



Lt. ☉ Ft. 14

+4.1 +1.4 -1.3 -0.1 0.0 +0.4 +0.2 -0.6 +0.6 +0.3
 52 73 106 94 93 89 91 99 87 9.0
 25 20 14 5 3 18 16 17 20 25

+2.3 +0.7 -0.7 +0.1 -0.2 0.0 0.0 -1.3 -0.2 -0.7
 73 59 77 65 68 6.6 6.6 7.3 6.8 7.3
 25 21 18 15 9 5 13 16 19 25

-0.2 -1.2 -0.4 +0.1 0.0 +0.1 -0.2 -0.8
 71 81 73 68 69 6.3 7.7 7.7
 14 11 10.8 8 12 19
 Ft.

+1.8 -0.5 -1.8 -1.5 -0.1 -0.5 0.0 +0.4 +0.3 -1.0 -0.5 -1.0
 63 91 104 101 87 91 8.6 8.2 8.3 9.0 9.1 9.6
 25-23 13 14 13 9 8 4 10 16 19 25

+0.8 -1.8 -1.5 -0.2 -0.6 0.0 0.0 -1.7
 61 87 84 71 75 6.2 6.7 8.6
 25-21 17 14 9 3 12 16-25

+0.9 -1.6 -0.1 -0.4 0.0 +0.2 -1.3 -1.6 -2.2
 47 72 51 60 5.6 5.8 7.5 7.2 7.8
 25-21 17 10 3 11 16 20 25

+0.5 -0.4 -1.2 -0.7 -0.1 -0.4 0.0 +0.3 -1.5 -0.1 +0.2
 36 45 50 48 42 45 4.1 3.8 5.6 4.3 3.2
 25 20 17 14 9 4 10 15 18 25

Sta. B.S. 1006 36 F.S. Elev
 T.P. 6.31 1010.14 253 1003.83

B.M. #3 4.39 ^{1045.54} 1005.55

21 5.9 04.2

22 4.7 05.4

23 4.4 05.7

227944 9 pipe (Remains)

24 3.4 06.7

25 2.3 07.8

On N. root 24" E.I.H. 28' Pt. Sta 2045

+2.7 +3.1 -0.2 -1.2 -0.8 -0.1 -0.8 00 0.0 -0.1 -0.9 +1.3 +1.2
 $\frac{3.0}{25} \frac{2.8}{21} \frac{0.1}{18} \frac{7.1}{15} \frac{0.1}{13} \frac{6.3}{9} \frac{6.7}{7} 5.9 \frac{5.9}{10} \frac{6.0}{12} \frac{6.8}{14} \frac{4.6}{18} \frac{4.1}{25}$

+0.9 +0.6 -1.0 -0.4 +0.1 -0.4 00 +0.2 -1.1
 $\frac{3.8}{25} \frac{4.1}{21} \frac{5.7}{17} \frac{5.1}{14} \frac{4.6}{9} \frac{5.1}{7} 4.7 \frac{4.5}{11} \frac{5.8}{15} \frac{2.5}{25}$

-0.4 +0.2 -0.7 -0.2 +0.2 -0.1 00 +0.2 0.0 +0.2 -1.5 -1.8 -2.1
 $\frac{4.7}{25} \frac{4.2}{22} \frac{5.3}{15} \frac{4.6}{12} \frac{4.5}{8} \frac{4.1}{7} 4.1 \frac{4.7}{7} \frac{4.1}{8} \frac{4.2}{11} \frac{5.2}{14} \frac{6.5}{15} \frac{6.5}{25}$

same section as 23

+0.6 +1.2 +0.9 -0.8 -0.5 -0.4 00 +0.1 -1.3 -0.3 -0.4
 $\frac{2.0}{25} \frac{2.2}{22} \frac{2.5}{19} \frac{4.2}{15} \frac{3.5}{9} \frac{3.8}{7} 3.9 \frac{3.3}{11} \frac{4.1}{15} \frac{3.7}{18} \frac{3.8}{25}$

+3.7 +1.8 -0.6 -0.2 -0.4 -0.9 -0.4 00 -0.2 -0.7 -0.2
 $\frac{1.4}{25} \frac{0.6}{19} \frac{2.0}{14} \frac{2.5}{12} \frac{2.7}{8} \frac{3.2}{7} \frac{2.7}{3} 2.9 \frac{2.5}{14} \frac{3.2}{16} \frac{2.5}{19} \frac{2.5}{25}$

Sta. H. I. F.S. Elev.

B.S. 1010 1A 2,12 1008.02

T.P. 4.27 1012 29 3.3 09.0

26 3.6 08.7

27 5.2 07.1

28 7.3 05.0

+25 7.7 04.6

29 7.2 05.1

+54 L. Stone Box Culv.
3' X 3' 1/2
Excellent Cond

30 4.9 07.4

✓

Lt. ϕ Rt. 16

+2.0 +0.8 +0.4 0.0 -0.3 -0.1 -0.6 -1.8
 $\frac{1.6}{25} \frac{2.2}{12} \frac{3.2}{6} \frac{3.2}{3} \frac{3.9}{9} \frac{3.7}{14} \frac{4.2}{17} \frac{5.4}{25}$

+2.1 +0.7 -0.4 -1.3 -0.4 -0.8 -0.3 0.0 -0.3 -0.8 -0.8 -1.7
 $\frac{3.1}{25} \frac{4.5}{20} \frac{5.6}{16} \frac{6.5}{14} \frac{6.0}{10} \frac{5.5}{6} \frac{5.2}{3} \frac{5.5}{8-13} \frac{6.0}{15} \frac{6.0}{18} \frac{6.3}{25}$

+3.0 +0.9 +0.1 -0.5 -0.3 0.0 0.0 -1.7 -1.6 -0.3
 $\frac{4.0}{25} \frac{6.4}{20} \frac{7.2}{16} \frac{7.8}{14} \frac{7.6}{10} \frac{7.0}{7} \frac{7.3}{10} \frac{9.2}{16} \frac{8.9}{19} \frac{7.6}{22-25}$

2.5 -1.7 -0.6 0.0 0.0 +0.2 -1.8 -3.5 -4.7
 $\frac{8.7}{25} \frac{9.1}{18} \frac{7.8}{10} \frac{7.2}{8} \frac{7.2}{7} \frac{7.0}{8} \frac{9.0}{12} \frac{10.1}{19} \frac{11.0}{25}$

18' 12'

-3.8 -3.1 -1.8 -0.1 0.0 +0.4 -1.4 -2.9 -3.3
 $\frac{8.7}{25} \frac{1.6}{20} \frac{6.7}{16} \frac{5.0}{11} \frac{1.7}{7} \frac{4.5}{8} \frac{6.3}{12} \frac{7.8}{19} \frac{8.5}{25}$

Sta B.S. H. I. F. S. Elev.
 31 1012 29 0.2 12.1

T.P. 12.15 1024 28 0.16 1012.13

32 6.2 18.1

33 9.3 24.0

T.P. 10.26 1034 08 0.16 1023.82

34 5.8 28.3

T.P. 10.60 1043 08 1.0 1032.48

35 10.6 32.5

36 6.1 37.0

T.P. 7.50 1046 81 3.77 1039.31



17

-1.7 -1.5 -0.3 -0.5 0.0 -0.3 0.0 10.2 2.2 1.1 1.2
 $\frac{12}{25} \frac{17}{26} \frac{9.5}{9} \frac{6.7}{4} 0.2 \frac{0.5}{3} \frac{0.2}{2} \frac{0.0}{10} \frac{2.4}{14} \frac{1.6}{17} \frac{1.07}{17} \frac{2.8}{25} \frac{0.5}{25}$

+4.5 -0.5 -0.2 +0.1 -0.4 0.0 -0.1 +0.1 -0.6 +1.6 +1.8
 $\frac{11.7}{25} \frac{6.1}{17} \frac{6.4}{15} \frac{6.1}{9} \frac{6.6}{5} \frac{6.2}{5} \frac{6.3}{8} \frac{6.1}{13} \frac{6.8}{13} \frac{4.6}{20} \frac{4.4}{25}$

+3.3 +0.3 -0.5 +0.3 -0.4 0.0 +0.2 -0.4 +4.7
 $\frac{-3.0}{25} \frac{0.0}{26} \frac{0.0}{15} \frac{0.0}{12} \frac{0.7}{9} \frac{0.3}{4} \frac{0.1}{12} \frac{0.7}{14} \frac{-4.7}{21} \frac{-4.7}{25}$

+4.3 +2.7 +0.7 -0.3 +0.2 -0.3 0.0 +0.1 -0.6 +2.0 +3.2
 $\frac{6.3}{25} \frac{3.1}{20} \frac{3.1}{14} \frac{6.1}{12} \frac{5.6}{8} \frac{6.1}{4} \frac{5.8}{4} \frac{5.7}{2-11} \frac{6.9}{14} \frac{3.8}{18} \frac{2.6}{20} \frac{2.6}{25}$

+1.9 +0.9 -1.4 +0.1 0.0 -0.3 +0.1 -0.9 +0.6 +4.1 +4.3
 $\frac{8.7}{25} \frac{5.1}{26} \frac{12.0}{11} \frac{10.5}{9} \frac{10.6}{9} \frac{10.9}{3} \frac{10.5}{11} \frac{11.5}{14} \frac{10.0}{17} \frac{6.5}{17} \frac{6.5}{25}$

+1.8 +1.3 -0.3 -0.4 -0.7 0.0 -0.3 -0.1 -1.0 -0.3 +1.3 +1.7
 $\frac{12.4}{25} \frac{6.4}{14} \frac{6.5}{17} \frac{6.8}{7} \frac{6.1}{3} \frac{6.4}{7} \frac{6.2}{10} \frac{7.1}{14} \frac{6.1}{16} \frac{4.8}{19} \frac{7.9}{25}$

1046 81

37. 7.6 39.2

+0.1	-0.8	0.0	-0.4	0.0	-0.2	+0.2	-0.6	-1.0
7.5	8.4	7.6	8.0	7.0	7.8	7.4	8.2	8.9
<u>25</u>	<u>16</u>	<u>5</u>	<u>4</u>		<u>6</u>	<u>9</u>	<u>12</u>	<u>25</u>

38. 6.8 40.0

+0.1	-0.2	-0.5	-0.2	+0.2	+0.1	0.0	-0.1	+0.2	-0.8	-1.6
6.4	7.0	7.3	7.0	6.6	6.7	6.8	6.7	6.6	7.6	8.1
<u>25</u>	<u>18</u>	<u>16</u>	<u>12</u>	<u>10</u>	<u>6</u>		<u>5</u>	<u>9</u>	<u>12</u>	<u>25</u>

39. 5.9 41.4

+1.0	-0.7	0.0	-0.3	0.0	+0.2	-0.4	-1.6
4.4	6.1	5.4	5.7	5.7	5.2	5.8	7.0
<u>25</u>	<u>16</u>	<u>13</u>	<u>8</u>		<u>10</u>	<u>13</u>	<u>25</u>

40. 3.5 43.3

+0.2	-0.2	+0.5	0.0	+0.4	-1.7	-0.8	-1.3
3.0	3.7	3.0	3.5	3.1	5.2	4.3	4.8
<u>25</u>	<u>14</u>	<u>8</u>		<u>9</u>	<u>14</u>	<u>16</u>	<u>25</u>

41. 0.2 46.6

+1.2	+0.6	-1.2	-0.9	+0.2	-0.3	0.0	-0.2	-0.1	-1.6	+1.2
-1.0	-0.1	1.4	1.1	0.0	0.5	0.2	0.4	0.3	1.8	-1.0
<u>25</u>	<u>23</u>	<u>18</u>	<u>14</u>	<u>10</u>	<u>6</u>		<u>8</u>	<u>12</u>	<u>15</u>	<u>16-25</u>

T.P. 10.31 1056.93 0.19 1048.02

42. 6.5 50.4

+1.8	+0.9	-0.2	+0.1	-0.1	0.0	+0.5	+0.1	-0.7	+0.1
4.7	5.6	6.7	6.1	6.0	6.5	6.0	6.4	7.2	6.4
<u>25</u>	<u>19</u>	<u>14</u>	<u>8</u>	<u>13</u>		<u>2</u>	<u>14</u>	<u>18</u>	<u>21-25</u>

43. 2.7 54.2

+0.7	-0.6	-0.3	+0.1	-0.4	0.0	+0.3	-0.6	-1.7	-1.3	-1.8
1.8	2.3	3.0	2.6	3.1	2.7	2.4	2.3	4.4	4.0	4.6
<u>25</u>	<u>13</u>	<u>9</u>	<u>6</u>	<u>3</u>		<u>2-11</u>	<u>15</u>	<u>18</u>	<u>20</u>	<u>25</u>

B.M.A 3.21 1053.75 1053.72

On NW root twin Elm 2.5' Rt. 5' 9' 43' 10'



T.P. 11.56 1066.66 1.83 1055.10

44 8.9 57.8

45 3.5 63.2

T.P. 10.50 1076.77 0.39 1066.27

46 6.7 70.1

T.P. 7.05 1082.55 1.27 1075.50

47 4.8 75.8

47.5 4.8 78.4

48 4.1 78.5

T.P. 4.73 1083.53 3.75 1079.80

+3.0 +1.7 +0.6 -0.5 +0.3 -0.2 0.0 +0.6 +0.7 -0.5 +0.2
59 70 83 94 86 21 89 83 82 94 87
28 18 14 11 7 4 4 13 17 21-25

+4.5 +0.5 +0.2 +0.9 +0.4 0.0 +0.7 +1.0 +0.9 +0.2 +2.1
-10 0.0 33 26 31 35 28 25 26 33 1A
25 19 13 10 4 2 8 15 17 19-25

+4.2 +3.9 +1.0 -0.6 -0.1 -0.2 0.0 +0.3 +0.6 -0.1 +2.8
25 28 57 73 68 67 67 64 61 68 39
25 20 16 12 9 6 3 11 16 20-25

+2.3 +6.8 +3.6 +1.5 -0.3 -0.5 0.0 +0.2 +0.4 +3.6 +5.2 +5.5
-1.5 0.0 32 53 71 73 68 66 64 32 16 1.3
25 22 20 15 11 6 4 9-13 17 19 25

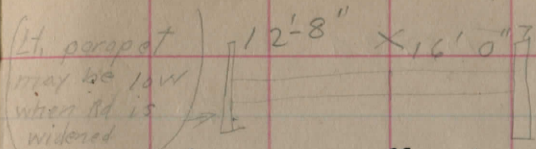
+12.2 +0.8 +4.2 +1.8 -0.1 +0.2 0.0 +0.3 +0.5 +0.1 +2.4 +7.6
-80 -10 21 43 40 42 39 37 41 18 -37
30 24 17 14 9 6 6 12 16 19 23-25

+9.8 +9.4 +17 -0.6 +0.3 0.0 +1.6 +0.4 -0.6 +4.1 +5.6
-57 -53 22 47 38 11 35 37 47 00 -15
25 23 14 10 6 9 13 17 21 22-25

+CO. bank ends
" " Fill begins
+50 bank ends
" " Fill begins.

1083 53

+49 & Culv. Stone 52 78.3
2 1/2 x 2 Box
Good



-7.7	-2.0	-0.1	-0.3	0.0	+0.4	-0.2				
12.9	7.2	5.3	5.5	5.2	4.8	5.4	Loads at			
7.8	12	7	4		9	7.6	Full			
FL										

-5.5	-5.6	-3.2	-0.2	-0.5	0.0	-0.3	-0.1	-1.1	-3.6	-7.5	-13.8
10.7	10.8	8.4	5.4	5.7	5.2	5.0	5.3	6.3	8.8	13.1	19.0
2.5	2.1	1.2	6	3		8	9	1.2	1.7	2.5	3.0

49 5.2 78.3

50 5.2 78.3

+0.7	0.0	-1.1	-0.5	+0.1	0.0	+0.2	+0.2	-1.3	-4.8
7.5	5.3	6.3	5.7	5.1	5.2	5.0	5.0	7.1	10.0
2.5	2.1	1.4	9	5		3	1.2	1.7	2.5

51 3.8 79.7

+5.1	+4.1	+3.1	+0.8	+0.2	0.0	+0.7	+0.6	-0.4	-1.5	-0.8
-1.3	-0.3	0.7	3.0	3.6	3.8	3.1	3.2	4.2	5.3	4.6
2.5	1.8	1.6	1.2	5		4	1.3	1.7	2.1	2.5

T.P. 6.75 1087 2.9 3.04 1080.89

52 6.0 81.2

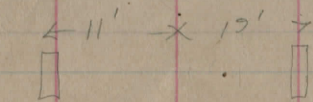
+1.4	+3.4	+1.2	+0.4	+0.1	0.0	+0.3	+0.3	-0.1	-0.7	-1.1	-0.1
1.0	2.6	4.8	5.6	5.9	6.0	5.7	5.7	6.1	6.9	7.1	6.1
2.5	1.9	1.4	7.0	7		4	1.3	1.2	2.0	2.3	2.8

53 5.3 81.9

-0.1	-0.9	-0.8	0.0	0.0	0.0	-1.1	-1.6
5.4	4.2	4.1	5.3	5.3	5.3	6.7	6.9
2.5	1.5	1.8	5		1.3	1.6	2.5

+60 & Culv. 15" V.I.P. & C.I.P. 4.9 82.3 ✓

Stone on Top of Pipe for end walls



-3.4	-1.3	0.0	+0.1	0.0	-2.3	-4.2	-3.7
8.3	6.2	4.9	4.8	4.9	7.2	9.1	8.6
FL	10		2	1.3	1.9	2.0	2.6
FL					FL	FL	FL

Sta

1087.2A

54

4.6 82.6

55

2.0 85.2

T.P. 11.96 1098.86

0.34 1086.90

56

10.9 88.0

57

9.3 89.6

58

6.6 92.3

10-25-12
cool - fair

B.M.#5 4.16 1100 76

2.25 1096.60
1096.61

59

5.3 95.5

+30

5.0 95.8
✓

Lt. £ Rt.

21.

-1.8	-1.0	-1.5	0.0	+0.2	0.0	+0.3	+0.2	-1.5	-2.1	+0.7
6.7	5.6	6.1	4.6	4.4	4.6	4.3	4.4	6.1	6.7	3.9
25	14	11	7	3		3	13	17	21	25

+2.0	+1.1	-0.3	-0.8	-0.1	-0.8	0.0	+0.3	+0.2	-1.3	-1.5	+0.2
0.5	0.9	2.3	2.8	2.1	2.8	2.0	1.7	1.8	3.3	3.5	1.8
25	19	16	11	8	4		3	14	18	20	25

+1.8	+1.4	-0.2	-0.5	-0.3	-0.5	-0.3	0.0	+0.4	0.0	-0.8	-0.7
0.1	0.5	1.1	1.4	1.2	1.4	1.2	1.0	1.5	1.0	1.7	1.6
25	16	13	10	5	3	2		4	16	18	25

+4.0	+3.4	+2.7	+0.5	-0.2	+0.3	0.0	+0.7	+0.4	-0.3	+0.3	+1.6
5.0	5.9	7.1	8.2	9.5	9.0	9.3	8.6	8.9	9.6	9.0	7.7
25	18	15	12	9	4		3	16	18	20	25

+3.4	+2.8	+1.1	+0.2	+0.4	0.0	-0.2	+0.7	+0.4	-0.2	+0.8	+1.1
3.2	3.8	5.5	6.4	6.2	6.6	6.8	5.3	6.2	6.8	5.8	5.5
25	15	12	8	5		2	4	16	18	21	25

04" N. root 36" Maple 40' Rt. Sta 62+45

+3.8	+3.2	-0.1	0.0	+0.2	+0.1	-0.2	+0.1
1.5	2.1	5.4	5.3	5.1	5.2	6.5	5.2
25	16	8		5	14	19	25

range Sec.
5.0

H. I.
Sta. B.S. 110076 F.S. Elev.
60 53 95.5

+76: $\pm 12''$ C.I.P. 57 95.1

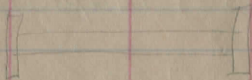
61 55 95.3

62 47 96.1

63 48 96.0

$\angle 11 \times 13'6''$

+98



2 1/2 x 3 stone

good cond., no floor.

64 AB 96.5

✓

Lt.

\pm

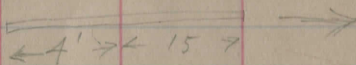
Rt.

22

+2.1	+1.1	+0.4	-0.9	+0.3	00	+0.6	-0.3	-1.2	0.0
3.2	4.2	4.9	6.2	5.0	5.3	4.7	5.0	6.5	5.3
2.5	2.8	1.5	7.1	6		4-13	7.6	2.0	2.5

-0.4	-0.9	-1.4	-0.4	00	+0.1	-0.4	-1.1	-1.5	-2.3
6.1	6.6	7.1	6.1	5.7	5.6	4.1	6.8	7.2	8.0
1.7	1.1	5	4		2	7.4	1.5	FL	2.0

FL
Rock



+0.4	-0.6	-1.0	-0.2	00	-0.4	-1.2	-1.4
5.1	6.1	6.5	5.7	5.5	5.9	6.7	6.2
2.5	1.8	1.2	9		7.4	7.6	2.5

+1.1	+0.5	-0.9	-0.2	00	+0.3	+0.1	-0.5	-0.1	0.0
3.6	4.2	5.0	4.9	4.7	4.4	4.6	5.2	4.8	4.7
2.5	1.5	1.1	6	6.0	3	1.2	1.6	1.7	2.5

+1.0	+0.8	+0.4	-0.8	-0.1	00	-0.2	-0.6
3.8	4.0	4.1	5.6	4.9	4.8	5.0	5.4
2.5	2.2	1.8	1.1	6		7.4	7.6-2.5

same as
Sta 64

-1.8	-4.5	+0.7	-0.5	00	+0.1	+0.7	-4.0	-3.4
6.1	8.8	3.6	4.8	4.3	4.2	3.6	8.3	7.7
2.5	1.2	1.1	9		1.2	13.6	7.4	2.5

FL
Par

1100 76

65 34 97.4

T.P. 8.78 1106 96 2.58 1098.18

66 83 98.7

67 69 00.1

68 53 07.7

69 35 03.5

T.P. 1024 1114⁵⁰ 99 2.21 1104.75

70 98 05.2

71 76 07.4



+0.1	-0.4	-0.7	0.0	0.0	+0.4	-0.5	+0.1
<u>3.3</u>	<u>3.8</u>	<u>4.3</u>	<u>3.4</u>	<u>3.7</u>	<u>3.0</u>	<u>3.2</u>	<u>3.3</u>
25	21	14	12	7	13	15	25

0.0	-0.3	-0.7	+0.1	0.0	+0.5	+0.7	+0.1	+0.5
<u>8.3</u>	<u>8.6</u>	<u>9.0</u>	<u>8.2</u>	<u>8.3</u>	<u>7.8</u>	<u>7.6</u>	<u>8.2</u>	<u>7.8</u>
25	12	10	7		4	15	17	25

+0.2	-0.2	-0.5	+0.1	0.0	+0.3	+0.3	-0.6	+0.4
<u>6.7</u>	<u>7.1</u>	<u>7.4</u>	<u>6.8</u>	<u>6.9</u>	<u>6.6</u>	<u>6.6</u>	<u>7.5</u>	<u>6.5</u>
25	14	10	5		4	15	17	25

+1.0	+1.2	+0.5	-0.5	+0.1	0.0	+0.1	-0.5	+0.3	+0.7
<u>4.3</u>	<u>4.1</u>	<u>4.8</u>	<u>5.8</u>	<u>5.2</u>	<u>5.3</u>	<u>5.2</u>	<u>5.8</u>	<u>5.0</u>	<u>4.6</u>
25	20	14	11	5		15	16	18	25

+1.1	+0.6	-0.4	+0.1	0.0	+0.5	+0.4	-0.8	-0.1	+0.4
<u>2.4</u>	<u>2.7</u>	<u>3.2</u>	<u>3.4</u>	<u>3.5</u>	<u>3.0</u>	<u>3.1</u>	<u>4.2</u>	<u>3.6</u>	<u>3.1</u>
25	13	10	5	80	5	14	17	19	25

+1.4	+0.6	-0.3	+0.2	0.0	+0.3	+0.4	-1.4	-0.6	+0.1
<u>9.4</u>	<u>8.2</u>	<u>10.1</u>	<u>9.6</u>	<u>9.8</u>	<u>9.5</u>	<u>9.4</u>	<u>11.2</u>	<u>10.4</u>	<u>9.7</u>
25	15	9	4		4	14	17	19	25

+1.5	+1.4	+0.2	-0.3	+0.5	0.0	+0.3	+0.5	-0.3	-1.0	+0.1	+0.5
<u>6.1</u>	<u>6.2</u>	<u>7.4</u>	<u>7.8</u>	<u>7.1</u>	<u>7.6</u>	<u>7.3</u>	<u>7.1</u>	<u>7.9</u>	<u>8.4</u>	<u>7.5</u>	<u>7.1</u>
25	22	15	11	9		3	12	14	10	19	25

Sta.

1114.99

72

5.0

10.0

RM#6

3.55

1111.44

73

2.8

12.2

74

1.8

13.2

T.P.

5.09

1118.61

1.47. 1113.52

75

5.2

13.4

76

4.8

13.8

77

5.2

13.4

78

6.0

12.6

24

+1.6	+1.3	+1.1	-0.3	-0.1	0.0	+0.5	+0.6	-0.3	+0.2	+0.8
3.7	3.7	4.6	5.3	5.1	5.0	4.5	4.4	5.3	4.8	4.2
2.5	1.5	1.2	9	7	0.0	3	1.3	7.6	7.9	2.5

Nail in N.E. root 30" Maple 35' RT STA 72+5

+0.5	+0.4	-0.6	-0.2	0.0	+0.4	+0.6	-0.3	+0.6
2.3	2.4	3.4	3.0	2.8	2.4	2.7	3.1	2.7
2.5	1.2	1.0	8	0.0	3	1.3	1.5	1.7

+0.3	-0.9	0.0	0.0	+0.4	+0.5	-0.4	+0.1	+0.3
1.5	2.7	1.3	1.8	1.4	1.3	2.2	1.7	1.5
2.5	1.4	1.1	1.7	0.0	8	1.3	1.6	1.7

-0.3	-0.8	-0.4	0.0	+0.3	+0.7	-0.3	+0.1	+0.4
3.5	6.0	5.5	5.2	4.3	4.5	3.5	3.1	4.8
2.5	1.1	8	0.0	4	1.3	1.5	1.7	2.5

+0.1	-0.4	0.0	0.0	+0.3	+0.5	-0.3	+0.5	+0.8
4.7	5.2	4.8	4.8	4.5	4.3	5.1	4.3	4.0
2.5	9	7		7	1.3	1.5	1.7	2.5

+0.5	+0.1	-0.1	-0.5	-0.2	0.0	+0.4	+0.5
4.7	4.1	5.3	5.7	5.4	5.7	4.8	4.7
2.5	2.2	1.3	1.0	8	1.3	2.5	

-0.1	-0.3	-0.5	-1.1	-0.3	0.0	+0.5	+0.7	-1.3	+0.1	+0.4
6.1	6.3	6.5	7.1	6.3	6.0	5.3	5.3	7.3	5.9	5.5
2.5	1.6	1.1	8	6	0.0	1.5	1.5	1.9	2.2	2.5

Sta. 79 1118.61
6.0 12.6

+32 2'x2' Stone Cully
Good Corrd. No floor 5.1 13.5

80 5.5 13.1

81 4.8 13.8

82 3.8 14.8

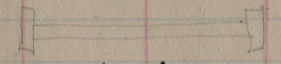
T.P 7.45 1122.7 6.8 3.28 1115.23

83 6.8 15.9

84 5.5 17.2



-0.6 -0.7 -1.4 -0.3 0.0 +0.6 +0.8 -0.4 -1.5 -0.7 -0.5
 6.6 6.9 7.4 6.3 6.0 5.4 5.2 6.4 7.5 6.7 6.5
 25 12 10 6 0.0 7 13 15. 18 20 25
 4 4 RT
 ← 10'9" x 15'9" →



-3.5 +1.2 +0.1 0.0 +0.3 +1.1 -3.2 -2.7
 8.6 3.9 5.0 5.1 4.8 4.0 8.3 7.7
 11 10 9 20 7-14 15 16 22
 Min Par

-0.5 -1.3 -0.5 0.0 +0.6 -1.5 -0.6 -0.5
 6.0 6.8 6.0 5.5 4.9 4.0 6.1 6.0
 25-10 8 6 7-13 17 20 25

-0.4 -0.3 -1.2 -0.4 0.0 +0.5 +0.7 -1.3 -0.6 -0.5
 5.2 5.1 6.0 5.2 4.8 4.3 4.1 6.1 5.9 5.3
 25 12 10 8 7 13 17 20 25

-1.0 -0.8 -1.5 -0.7 0.0 +0.2 +0.4 -1.2 -1.3 -0.9
 4.8 4.6 5.3 4.5 3.8 3.6 3.4 5.0 5.1 4.7
 25 11 9 8 6 12 15 18 25

-1.1 -0.7 -1.6 -0.5 0.0 +0.4 -1.3 -0.6 -0.9
 7.5 7.7 8.4 7.3 6.8 6.4 8.1 7.4 7.7
 25 12 10 7 6-12 15 18 25

-1.2 -0.8 -1.6 -0.6 0.0 +0.5 -1.4 -0.7 -0.9
 6.1 6.3 7.1 6.1 5.5 5.0 6.7 6.2 6.4
 25 13 11 9 8 11 15 16 25

Sta

1122⁷ 68

85

4.1 18.6

86

2.1 20.6

T.P.

12.12 1133⁸ 79

1.08 1121.60

87

7.9 23.5

88

9.1 24.7

89

6.6 27.2

90

4.1 29.7

91

1.9 31.9

T.P.

8.99 1141 34

1.44 1132.35

✓

26

-0.4	-0.7	-1.6	-0.7	0.0	+0.3	+0.1	-1.5	-0.2	-0.1
7.5	4.8	5.7	4.8	4.1	3.8	4.0	5.6	4.3	4.2
2.5	1.4	1.2	0.9	0.0	0.5	1.1	1.4	1.6	2.5

+0.5	+0.4	-1.1	-1.5	-0.8	0.0	+0.5	-1.1	-1.7	+0.4
1.6	1.7	3.2	3.6	2.9	2.1	1.6	3.2	3.8	1.7
2.5	1.9	1.3	1.8	0.8		0.9	1.2	1.4	1.2

+1.2	+0.5	-1.0	-0.6	0.0	0.0	-1.4	+0.3	+1.4
9.7	10.4	11.2	11.5	10.9	10.2	12.3	10.1	9.5
2.5	2.1	1.5	1.6	0.0	1.0	1.2	1.5	2.5

+1.5	+0.8	-0.9	0.0	+0.2	-0.2	-1.2	-0.5	+2.1	2.5
7.6	8.3	10.0	9.1	8.7	8.3	10.3	9.6	7.0	6.6
2.5	1.6	1.2	0.8	0.5	1.0	1.2	1.5	1.8	2.5

+0.9	+0.6	-0.7	-0.9	0.0	+0.3	-1.8	+0.3	+1.5
5.7	6.0	7.3	7.5	6.6	6.3	8.4	6.3	5.1
2.5	1.4	1.2	0.8	0.0	0.8	1.2	1.4	2.5

+0.2	+0.1	-0.9	-0.8	0.0	+0.2	+0.1	-1.4	+0.5	+1.1
3.2	4.0	5.0	4.7	4.1	3.9	4.0	5.5	3.6	3.0
2.5	1.4	1.2	0.7		0.7	0.9	1.1	1.2	2.5

0.0	-0.5	-1.1	-0.8	0.0	+0.2	-0.1	-1.4	-0.6	+0.7
1.0	2.4	3.0	2.7	1.9	1.7	2.0	3.3	2.5	1.2
2.5	1.5	1.8	0.8	0.0	0.4	0.9	1.1	1.5	2.5

114134

92 7.7 33.6

-0.5 -0.4 -1.0 -0.8 0.0 +0.3 0.0 -1.1 +0.3 +0.5
8.2 8.1 8.7 8.5 7.7 7.4 7.7 8.8 7.4 7.2
2.5 1.6 1.2 1.8 1.7 1.4 1.9 1.1 1.6 2.5

93 6.4 34.9

-0.2 -0.4 -0.9 -0.5 0.0 +0.2 -0.1 +0.7
6.6 6.2 7.3 6.2 6.4 6.2 6.5 5.7
2.5 1.6 1.8 1.8 0.0 1.3 1.8-1.0 2.5

94 4.6 36.7

-0.4 -0.5 -1.1 -0.8 0.0 0.0 -0.3 -1.0 -0.5 +0.4
5.0 4.7 5.7 5.4 4.6 4.6 4.9 5.6 5.1 4.7
2.5 1.9 1.4 1.8 1.3 1.7 1.1 1.7 2.5

95 4.3 37.0

-0.4 -0.3 -0.5 -0.6 0.0 +0.1 -0.1 -0.9 -0.2 +0.2
4.7 4.6 5.2 4.9 4.3 4.2 4.4 5.2 4.5 4.1
2.5 1.6 1.5 1.0 0.0 1.4 1.8 1.0 1.5 2.5

96 3.9 37.4

-0.6 -1.1 -0.9 -0.5 0.0 +0.3 -0.3 -1.1 -0.6 +0.2
4.5 5.0 4.8 4.4 3.9 3.6 4.2 5.0 4.5 3.7
2.5-2.3 1.3 1.2 1.1 1.7 0.0 1.4 1.9 1.4 2.5

97 4.7 36.6

-0.5 -0.7 -0.8 -0.2 0.0 +0.1 0.0
5.2 5.4 5.5 4.9 4.7 4.6 4.7
2.5 1.5 1.0 1.6 1.0 2.5

T.P. 2.73 1139 35 4.72 1136.62

B.M.#7 2.04 1137.34 1137.31

On N.E. root 20" Maple 35' Nt. str. 97+80

98 4.9 34.5

+1.0 +0.8 +0.1 -0.5 -0.3 0.0 +0.2 +1.0 +1.2
3.9 4.1 4.3 5.4 5.2 4.9 4.7 3.9 3.7
2.5 1.9 1.4 1.1 1.9 1.9 1.3 1.7-2.5

✓

H. I.
Sta B.S. 1139^A 35 F.S. Elev.

99

6.5

32.9

+0.9	+0.4	-1.0	-0.2	0.0	+0.1	-1.0	+0.9	+1.1
5.6	6.1	7.5	6.7	6.5	6.1	7.5	5.6	5.9
25	19	14	12	9	6	00	9	12
							45	25

100

8.0

31.4

+0.5	+0.2	-1.1	-0.3	0.0	-0.1	-0.9	-0.2	+0.6
7.5	7.8	9.1	8.3	8.0	8.1	8.9	8.7	7.4
25	14	11	8	00	10	12	16	25

101

10.4

29.0

+0.7	+0.2	-1.2	-0.3	0.0	0.0	-1.1	+0.4
9.7	10.2	11.6	10.7	10.4	10.8	11.5	10.0
25	21	14	11	8	00	9	17
					Gravel		25

T.P.

2.21

1130

51

11.05

1123.0

102

3.6

26.9

+0.5	+0.3	-0.4	-1.2	-0.5	0.0	-0.4	-1.5	-0.7	0.0	+0.8
3.1	3.3	4.0	4.8	4.1	3.6	4.0	5.1	4.3	3.6	2.8
25	17	13	10	8	00	8	10	12	15	25
					Gravel					

103

5.2

25.3

-0.5	-0.4	-1.0	-0.4	0.0	-0.3	-1.4	-0.2	+0.7
5.5	5.6	6.2	5.6	5.2	5.5	6.6	5.9	4.5
25	14	11	9	00	8	10	14	25
					Gravel			

104

6.5

24.0

-0.6	-0.3	-1.0	-0.4	0.0	-0.2	-1.2	0.0	+0.4
7.1	6.8	7.5	6.9	6.5	6.7	7.7	6.5	6.1
25	14	12	11	Gravel	7	9	11	25

105

8.0

22.5

-0.6	-0.1	-0.5	+0.3	+0.6	0.0	+0.5	+0.4	-0.6	+0.1	+0.3
8.6	8.1	8.5	7.7	7.1	8.0	7.5	7.6	8.6	7.9	7.7
25	16	14	11	4	00	4	8	10	13	25
					Gravel & mud					

✓

Lt.

±

Rt.

28

H. I.

Sta. B.S. 1130 51 F.S. Elev.

106 8.2 22.3

-0.5 -0.6 -1.1 -0.3 0.0 -0.7 -1.7 -0.3 0.0 -0.1
 $\frac{8.7}{25} \frac{8.8}{15} \frac{9.3}{13} \frac{8.5}{9} \frac{8.2}{00} \frac{8.9}{9} \frac{9.9}{11} \frac{8.5}{14} \frac{8.2}{19} \frac{8.3}{2.5}$
 dirt

107 98 20.7

+1.1 +0.4 -0.8 -0.4 0.0 0.0 -0.5 -1.1 -0.2 +1.1
 $\frac{8.7}{25} \frac{9.4}{17} \frac{10.6}{14} \frac{10.2}{12} \frac{9.8}{4} \frac{9.8}{00} \frac{10.3}{7} \frac{10.9}{8} \frac{10.0}{10} \frac{9.7}{2.5}$
 dirt

T.P. 3.31 1124 37 9.45 1121.06

108 4.9 19.5

+0.2 -0.2 -1.0 -0.2 0.3 0.0 0.0 -0.8 0.0
 $\frac{4.5}{25-20} \frac{5.1}{15} \frac{5.7}{13} \frac{5.1}{11} \frac{4.9}{5} \frac{4.9}{dirt} \frac{4.9}{8} \frac{5.7}{9} \frac{4.9}{10-2.5}$

+52 ϕ 12" C.I.P.

18' (?) pipe

Lt. end probably broken

5.2 19.2



-1.3 -1.0 -0.4 0.0 +0.5 -0.2 -1.5 -0.4
 $\frac{6.5}{17} \frac{6.2}{9} \frac{5.6}{6} \frac{5.2}{00} \frac{4.7}{0} \frac{5.4}{11} \frac{6.7}{12} \frac{5.6}{17}$
 FL mud

109 5.5 18.9

-0.5 -0.5 -0.1 +0.2 0.0 -0.1 -0.7 0.0 +0.6
 $\frac{6.0}{25-22} \frac{6.0}{19} \frac{5.6}{10} \frac{5.3}{3} \frac{5.5}{dirt} \frac{5.6}{9} \frac{6.2}{12} \frac{5.5}{14} \frac{4.9}{2.5}$

110 5.5 18.9

-0.5 +0.7 +0.5 -0.7 -0.2 +0.3 0.0 -0.6 -1.1 +0.4 +1.4
 $\frac{6.0}{25} \frac{4.3}{19} \frac{5.0}{15} \frac{6.2}{12} \frac{5.7}{9} \frac{5.2}{3} \frac{5.5}{00} \frac{6.1}{7} \frac{6.6}{9} \frac{5.1}{12} \frac{4.1}{2.5}$

111 7.4 17.0

-0.1 +0.2 +1.1 -0.3 +0.3 0.0 -0.8 -1.1 -0.2 +1.0 +2.2
 $\frac{7.5}{25} \frac{7.2}{16} \frac{6.3}{14} \frac{7.7}{10} \frac{7.1}{5} \frac{7.4}{00} \frac{8.2}{5} \frac{8.5}{7} \frac{7.6}{10} \frac{6.4}{12} \frac{5.2}{2.5}$



Sta.	B.S.	H. I.	F.S.	Elev.
112	1124	37	100	14.4
T.P.	0.29	1115	28	9.38
				1114.99

113			33	12.0
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113+00 ϕ 12" C.I.P. (reg)

114			80	07.5
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B.M.#8 7.11 1108.21
1108.17

T.P.	2A3	1107	26	10.45
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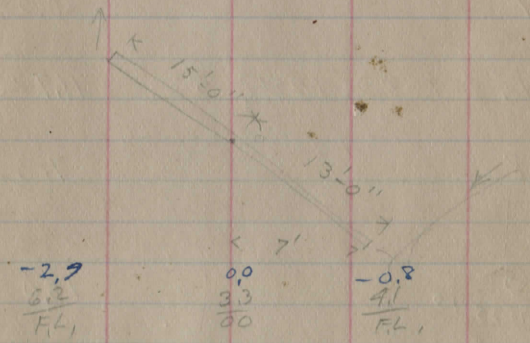


+0.2	+0.5	-1.1	-0.5	0.0	-0.5	-1.3	+1.1	+2.8
<u>98</u>	<u>95</u>	<u>11.1</u>	<u>105</u>	<u>10.0</u>	<u>10.5</u>	<u>11.3</u>	<u>8.9</u>	<u>7.2</u>
25	18	14	12	00	5	6-8	11	25

DIT

+0.7	+0.6	-0.6	-2.3	-1.4	-0.7	0.0	+0.3	+0.7	-0.1	+0.4	+2.7
<u>26</u>	<u>27</u>	<u>37</u>	<u>5.6</u>	<u>47</u>	<u>4.2</u>	<u>3.3</u>	<u>3.0</u>	<u>2.4</u>	<u>3.4</u>	<u>2.9</u>	<u>0.6</u>
25	19	16	14-13	12	10	7	16	19	24	26	

some slope



+1.2	+1.1	-0.4	-0.1	-1.3	-0.5	0.0	-0.2	-0.9	-1.3	+1.5	+2.2
<u>68</u>	<u>69</u>	<u>81</u>	<u>101</u>	<u>93</u>	<u>85</u>	<u>80</u>	<u>82</u>	<u>89</u>	<u>93</u>	<u>65</u>	<u>58</u>
25	21	15	13	10	6		6	11	14	17	26

some slope

on N.E. root end triple 23' RT, sta 114+35

1107 26

115 22 05.1

-0.5	-0.8	-0.1	-2.5	-1.4	-0.6	0.0	-0.6	-1.3	-2.0	-0.1	+2.6	+2.8
2.7	3.0	2.3	4.7	3.6	2.8	2.2	2.8	3.5	4.2	2.6	0.4	-0.6
25	21	18	14	11	7	00	7	10	13	15	19	25

coarse slag

116 5.9 01.4

+0.3	+1.1	-1.4	-2.4	-0.4	0.0	-0.7	-1.7	-0.3	+2.2	+3.4
5.6	4.8	7.3	8.3	6.3	5.9	6.6	7.6	6.2	3.7	2.5
25	20	17	15	10		8	11	13	12	25

same slag

117 10.3 97.0

-0.1	+0.3	+0.1	0.0	-0.7	-1.4	-0.5	+1.1	+2.8
10.4	10.0	10.2	10.3	11.0	11.7	7.8	9.2	7.5
25	17	10	00	9	12	14	13	25

same slag

T.P. 2.99 1098 53 11.72 1095.54

118 7.3 91.2

+1.1	+1.3	-1.6	-1.3	-0.6	0.0	-0.3	-1.2	-0.3	+4.3	+6.5
6.2	6.0	3.2	8.6	7.9	7.3	7.6	8.5	7.6	3.0	0.8
25	21	17	16	13	9	00	9	11	13	18

same slag

119 15.0 83.5

+0.6	+0.4	-1.2	-0.3	0.0	+0.4	-0.6	+1.8	+5.3
14.1	14.5	16.2	15.3	15.0	1.4	15.6	13.2	9.7
25	20	16	13	00	8	11	15	25

Rock

T.P. 0.48 10.87 11 11.90 1086.03

120 10.9 76.2

+1.5	+1.4	-1.6	-0.3	+0.4	0.0	+0.7	-0.2	+1.7	+3.7	+4.2
9.4	9.5	12.5	11.2	10.5	10.9	10.2	11.1	9.2	7.2	6.7
25	15	12	10	7		7	9	13	20	25

Rock

T.P. 1.00 1076.54 11.57 1075.54

121 6.8 69.7 ✓

+0.8	+0.7	-1.8	+0.2	0.0	+0.2	-1.5	+2.7	+3.8
6.0	5.9	8.6	6.6	6.8	6.6	8.3	4.1	3.0
25	20	15	14	11	7	10	14	25

gravel

1076 59

B.M.#

4.06 ^{1072.51} 1072.48

On N.E. root 12" Maple 25' Rt., Sta. 12(125)

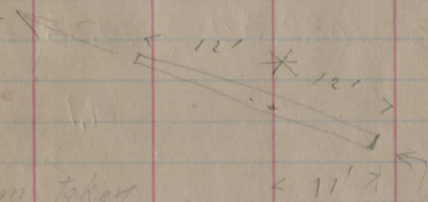
T.R 1.90 1068.39 10.05 1065.49

122 5.9 62.5

+1.1	+0.2	-0.8	+0.2	0.0	+0.7	-1.3	+1.5	+3.2	+4.1
<u>9.8</u>	<u>5.7</u>	<u>6.7</u>	<u>5.7</u>	<u>5.7</u>	<u>5.2</u>	<u>7.2</u>	<u>4.1</u>	<u>2.7</u>	<u>1.8</u>
25	-21	18	14.3	9	9	12	15	20	25

slay - gravel

+06 & 12" C.P.P.,
Solid, good Corrid.



Section taken

thru Cully

-2.5	-1.9	-1.0	+0.3	0.0	+0.4	-0.7
<u>9.9</u>	<u>8.7</u>	<u>7.5</u>	<u>6.2</u>	<u>6.5</u>	<u>6.1</u>	<u>7.2</u>
21	13	12	10	0.0	12	13 F.L.

pipe comes to surface east

T.P. 1.19 1059.08 10.00 1057.81

123 6.1 52.7

+2.2	+2.2	-0.7	-1.0	-0.3	0.0	-0.2	+0.1	-1.3	+0.3	+3.2	+6.3
<u>1.1</u>	<u>1.1</u>	<u>7.1</u>	<u>7.4</u>	<u>6.7</u>	<u>6.4</u>	<u>6.6</u>	<u>6.3</u>	<u>7.7</u>	<u>6.1</u>	<u>3.2</u>	<u>0.1</u>
25	21	15.4	13	8	slay	7	9	13	10	18	25

T.P. 2.37 1049.69 11.76 1047.32

12A 5.7 44.0

+3.8	+0.6	-0.8	+0.7	0.0	-0.1	-1.5	+0.2	+2.0	+5.1	+6.5	
<u>1.9</u>	<u>5.1</u>	<u>6.5</u>	<u>5.5</u>	<u>5.7</u>	<u>5.8</u>	<u>7.2</u>	<u>5.5</u>	<u>2.8</u>	<u>0.6</u>	<u>-0.8</u>	
25	23	19	16	5	6.0	6	9	10	14	18	25

102230

128 ~~75~~ 8.3 14.1
 T.P. 0.78 1016 40 6.68 1015.62

129 4.0 12.4

130 4.9 11.5

B.M. #0 Luatz New culv. 4.73 1015.67
 st 4 130 + 95

131 12" CI Pipe 18' 4.8 11.6

132 2.8 13.6

T.P. 6.25 1020 65 2.00 1019.90

+35 6.3 14.4

138 7.5 13.2

34

-4.0 +0.7 +0.4 0.0 0.0 -2.2 -2.6
~~12.2 9.3 8.8 8.2 8.2 10.4 10.8~~
~~25 21 15 10 00 7 15 25~~

+0.4 -1.1 -0.3 +0.4 0.0 0.0 +0.5 +1.8
~~3.6 5.1 4.3 3.6 4.0 4.0 3.5 2.7~~
~~25 25 19 16 12 7 10 25~~

-0.5 -0.3 -0.8 +1.2 0.0 -0.4 -0.2
~~5.1 5.2 5.7 4.7 4.9 5.3 5.1~~
~~25 19 16 14 10 9 25~~

On N.E. Foot 40" E/77 22' RT, Sta 130 + 50

-0.2 -0.6 -1.0 +0.1 0.0 0.0 -1.1 -0.9 -2.6
~~5.9 5.1 5.8 4.7 4.8 4.8 5.8 5.7 7.4~~
~~25 18 16 14 10 00 4 7 10 25~~

+0.1 -2.7 -1.3 -0.4 0.0 -0.3 -0.8 -0.3 0.0
~~2.7 2.5 4.1 3.2 2.8 2.1 3.6 3.1 2.8~~
~~25 16 14 13 11 00 5 7 9 25~~

+1.8 +0.8 -0.8 -0.2 0.0 -0.2 -0.8 +2.9 +4.9 +6.3
~~4.5 4.5 4.1 4.5 4.3 4.5 4.1 3.4 1.4 0.0~~
~~25 17 13 10 00 5 7 11 14 25~~

+4.5 +5.7 +3.5 -1.0 -0.4 0.0 -0.3 -0.8 +3.8 +4.4
~~3.0 1.8 4.0 8.5 7.9 7.5 7.8 8.3 3.7 3.1~~
~~25 18 18 7 4 00 10 12 17 25~~

1020 65

T50

10.2 10.5

T.P.

5.99 1016 70 9.88 1010 77

134

6.9 09.9

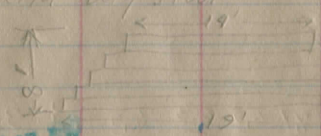
135

7.0 09.3

136

7.4 12.4

T21 W. end Bldg floor



W. about 4'

Sec. at W. end

3.5 13.3

E. About same as W. but has 7 tiers stone

4.4 14.92

Sec. at E. end

12.00 04.76
2.5 14.3

3.98 12.78
12.9 03.94

+0.1	-0.2	-0.9	-0.4	-0.3	0.0	40.7	+0.1	-0.9
40.1	11.1	11.6	10.6	10.5	10.2	7.7	10.1	11.1
25	20	17	8	1		13	21	25

-0.8	-1.2	-0.8	-0.4	0.0	+0.3	-0.4	-0.8
7.7	8.1	7.7	7.3	6.9	6.6	7.3	7.7
25	14	4	2		11	23	25

-0.5	-1.0	-0.2	0.0	+0.3	-0.3	-0.5	+0.1
7.5	8.0	7.2	7.0	6.7	7.3	7.5	6.8
25	12	5	00	8	16	19	25

-5.0	-5.5	-1.2	0.0	0.0	+0.2	-1.2	-1.8	-1.6
9.4	9.9	5.6	4.4	4.4	4.2	5.6	9.2	9.0
25	19	12	8	00	6	10	17	25

Very light
1000 bridge

<10' x 4' >

17' x 10' box
28' span

15' x 5' + 2'

-3.2	-0.4	0.0	0.0	+0.1	-0.3	-3.9	-8.1	9.4
6.7	3.8	3.5	3.5	3.4	3.8	7.4	11.6	12.3
11	10	8		3	6	8	17	25

Bdy. seat W. end

Creek bottom

-1.0	0.0	0.0	-0.3	-3.6	-5.5	-1.6
4.4	2.5	2.5	2.8	6.1	3.0	7.1
11	10	00	11	6	11	25

(+50)

Bdy. seat E. end
footing E. about

1016 76

T.P. 9.50 1025.18 1.08 1015.68
137 9.1 76.1

T.P. 11.90 1036.97 0.11 1025.07

138 11.9 25.1

139 2.6 34.4

T.P. 12.25 1047.72 1.50 1035.72

B.M. #11 3.13 1044.59

140 5.7 42.0
10-29-78 cold - Fair - Cloudy
P.M. 1990
Thompson

B.M. #11 9.90 1054.51 1044.61

141 7.9 46.6

141+60 5.8 42.7

11.90 1036.97
10.11 1025.07

-0.5 -1.0 -0.2 0.0 0.0 -0.6 -1.0 -1.6
9.6 18.1 9.3 9.1 9.1 10.5 10.1 10.7
25 20 17 10 5 15 2.5

+2.8 +0.2 -1.1 +0.6 +2.1 0.0 -0.1 -0.8 +0.9 +6.4 +7.1
9.1 11.7 13.0 11.7 11.8 11.7 12.0 12.1 11.0 5.5 3.8
25 22 20 16 13 4 5 8 15 25
High Bank Rt. begins 470

+4.6 +1.3 +0.5 -1.3 -0.6 -0.1 0.0 -0.2 -0.8 +1.8 +2.6 +5.3 +6.3
-2.0 1.3 2.1 3.7 3.3 2.7 2.6 2.8 3.9 0.8 0.0 -2.7 -3.7
25 20 17 16 14 9 6 8 12 13 15 25

On the roof 18" Evergreen in door yard Rt 139+30

+1.3 +1.0 -1.7 +0.1 0.0 +0.2 +1.2
4.4 4.7 7.1 3.6 5.7 5.3 4.5
25 19 15 12 12 2.5

+0.2 -0.7 0.0 2.0 -0.4 -0.8 -0.4 +0.1
7.7 8.6 7.9 7.9 8.3 8.7 8.3 7.8
25-16 11-2 10 5 7-1 12-14 16-25

+2.1 +1.8 -0.5 +0.1 0.0 -0.3 -1.1 -0.6 -0.1 +0.6 +0.9
3.7 4.0 6.3 5.7 5.8 6.1 6.9 6.9 5.5 5.5 4.9
25 18. 15-17 11 11 6 6 13 17 25

1054 51

142 4.0 50.5

T.P. 11.67 1065 52 0.66 1053.85

143 9.3 56.2

144 2.4 63.1

T.P. 12.16 1077 53 0.15 1065.37

145 6.5 71.0

T.P. 11.10 1086 34 2.29 1075.29

146 8.1 78.2

T.P. 11.30 1095 61 2.03 1084.31

147 10.2 85.4

T.P. 10.72 1104 70 1.63 1093.98

L₁ ⊕ R₁

37

$$\begin{array}{cccccccc}
 +3.2 & -0.7 & +0.2 & 0.0 & -0.1 & -0.7 & -0.5 & +1.4 & +2.1 \\
 0.2 & 4.7 & 3.8 & 1.0 & 4.1 & 4.2 & 4.5 & 2.4 & 1.2 \\
 \hline
 25-21 & 4-13 & 11 & & 5 & 8 & 9-12 & 16 & 25
 \end{array}$$

$$\begin{array}{cccccccc}
 +4.0 & -1.0 & -0.1 & 0.0 & 0.0 & -0.8 & -0.1 & +2.8 \\
 5.3 & 10.3 & 9.1 & 9.3 & 9.3 & 10.1 & 9.4 & 6.5 \\
 \hline
 25-22 & 15-13 & 12 & & 3 & 5-8 & 9-11 & 15-25
 \end{array}$$

$$\begin{array}{cccccccc}
 +5.0 & +2.4 & -1.0 & 0.0 & 0.0 & -0.2 & -1.2 & +2.4 & +3.2 & +3.9 & +3.2 \\
 -2.6 & 0.0 & 3.4 & 2.1 & 2.4 & 2.6 & 3.6 & 0.0 & -0.7 & -1.5 & -0.8 \\
 \hline
 25-23 & 21 & 15 & 12 & 2.4 & 4 & 7 & 10 & 15 & 18 & 25
 \end{array}$$

$$\begin{array}{cccccccc}
 +4.4 & -0.7 & +0.1 & 0.0 & -0.3 & -1.7 & -0.9 & +1.6 & +1.1 \\
 2.1 & 7.2 & 6.4 & 0.5 & 6.8 & 8.2 & 7.4 & 4.7 & 5.4 \\
 \hline
 25-22 & 16 & 14 & & 4 & 7 & 9-11 & 15 & 25
 \end{array}$$

$$\begin{array}{cccccccc}
 +3.0 & +1.7 & -1.7 & -0.2 & 0.0 & -0.3 & -1.6 & +0.2 & +1.4 & +0.9 \\
 5.1 & 6.4 & 9.8 & 8.3 & 8.1 & 8.4 & 9.7 & 7.2 & 6.7 & 7.2 \\
 \hline
 25-24 & 18 & 14-13 & 9 & & 2 & 6-8 & 9 & 13 & 2.5
 \end{array}$$

$$\begin{array}{cccccccc}
 +2.7 & -1.7 & -0.3 & 0.0 & -0.2 & -2.3 & +0.9 & +0.4 \\
 7.5 & 11.9 & 10.5 & 10.2 & 10.4 & 12.5 & 9.8 & 9.8 \\
 \hline
 25-21 & 15 & 11 & & 8.6 & 10-11 & 14 & 25
 \end{array}$$

1104 70

148

100 94.7

T.P. 12.24 1116 27

0.67 1104.0

149

11.2 05.1

BM #12

97.2 ^{1106.5} 1106.55

T.P. 1183 1127 26

0.89 1115.43

+75

13.2 14.1

150

11.3 16.0

151

3.4 23.9

T.P. 1140 1137 23

1.43 1125.83

152

5.2 32.0

$$\begin{array}{r} +2.8 \quad +2.1 \quad -1.8 \quad -0.2 \quad 0.0 \quad -0.4 \quad -1.3 \quad +0.3 \quad +0.5 \\ 7.2 \quad 7.9 \quad 11.8 \quad 10.2 \quad 10.0 \quad 10.4 \quad 11.3 \quad 9.7 \quad 9.5 \\ \hline 2.5 \quad 2.1 \quad 16.15 \quad 11 \quad 5 \quad 7 \quad 10 \quad 18.25 \end{array}$$

$$\begin{array}{r} +0.8 \quad -0.8 \quad -1.3 \quad -2.1 \quad -0.2 \quad 0.0 \quad -0.5 \quad -1.3 \quad -0.7 \quad +0.9 \quad +0.4 \\ 10.4 \quad 12.0 \quad 12.5 \quad 13.3 \quad 11.4 \quad 11.2 \quad 11.7 \quad 12.5 \quad 11.3 \quad 10.3 \quad 10.8 \\ \hline 2.5 \quad 2.2 \quad 20 \quad 18 \quad 15 \quad 4 \quad 2 \quad 8 \quad 15 \quad 2.5 \end{array}$$

on N.W. foot 18" Elm, 23' Pt. Ste. 142188

$$\begin{array}{r} +2.5 \quad 0.0 \quad -1.1 \quad -0.3 \quad 0.0 \quad -0.1 \quad -0.7 \quad +2.7 \\ 10.7 \quad 13.2 \quad 14.3 \quad 13.5 \quad 13.7 \quad 13.3 \quad 13.9 \quad 10.5 \\ \hline 2.5-2.3 \quad 1.6 \quad 15-14 \quad 11 \quad 6 \quad 8 \quad 15-2.5 \end{array}$$

Rock shows in 4 ditches

$$\begin{array}{r} +3.3 \quad +3.0 \quad -0.8 \quad -0.1 \quad 0.0 \quad -0.1 \quad -0.7 \quad +0.1 \quad +2.9 \quad +4.0 \\ 8.0 \quad 8.3 \quad 12.1 \quad 11.4 \quad 11.3 \quad 12.0 \quad 11.3 \quad 8.1 \quad 7.2 \\ \hline 2.5 \quad 2.0 \quad 7.4 \quad 11 \quad 0.0 \quad 5 \quad 6-7 \quad 9 \quad 12 \quad 15-2.5 \end{array}$$

Rock shows in ditches

$$\begin{array}{r} +2.9 \quad +1.4 \quad -1.0 \quad -0.3 \quad 0.0 \quad -0.1 \quad -0.7 \quad +2.8 \quad +5.1 \\ 9.5 \quad 2.0 \quad 4.4 \quad 3.7 \quad 3.4 \quad 3.5 \quad 4.1 \quad 0.6 \\ \hline 2.5-1.7 \quad 1.4 \quad 7.1 \quad 8 \quad 5 \quad 7 \quad 11 \quad 1.7 \quad 2.5 \end{array}$$

some rock

$$\begin{array}{r} +0.2 \quad -0.1 \quad -1.6 \quad -0.1 \quad 0.0 \quad -0.4 \quad -1.2 \quad +0.8 \quad +0.7 \\ 5.0 \quad 5.3 \quad 6.9 \quad 5.3 \quad 5.2 \quad 5.6 \quad 6.4 \quad 4.7 \quad 4.5 \\ \hline 2.5 \quad 2.2 \quad 1.0 \quad 9 \quad 8 \quad 10 \quad 13 \quad 2.5 \end{array}$$


1137 23

+25 3.6 33.6

T.P. 10.97 1147³ 29 0.91 1136.32

153 10.9 36.4

154 6.8 40.5

155 1.0 40.3

T.P. 11.08 1157⁶ 19 1.18 1146.11

B.M.#13 5.72 1151.45
1151.47

156 6.5 50.7

157 2.5 54.7

T.P. 6.27 1163 25 0.21 1156.97

-0.4 -1.0 -0.3 0.0 -0.5 -1.2 -0.2 +0.3
4.0 4.6 3.2 3.6 4.1 4.8 3.8 3.3
25-12 17-10 8 8 7 13 2.5

+0.3 -1.3 -0.3 0.0 -0.5 -1.4 +1.2
10.6 12.2 11.2 10.9 11.1 12.3 9.7
25-12 17-9 6 7 9 15-25

+1.6 +1.0 -1.5 -0.5 0.0 -0.5 -1.2 +2.2 +2.7
5.2 5.8 8.3 7.3 6.8 7.3 8.0 4.6 4.1
25 12 10-8 6 6 8 15 25

-0.1 -1.3 -1.9 -0.4 0.0 -0.5 -1.3 +2.3 +2.6
1.1 2.3 2.3 1.6 1.0 1.5 2.3 1.3 1.6
25 12 11 7 6 8 15 25

201 S. root 18" bitter nut 40' Lt 50' 55' +50
+1.7 +1.2 +0.1 -0.9 -0.2 0.0 -0.4 -0.8 +1.0 +2.8
4.8 5.3 6.1 7.4 6.7 6.5 6.2 7.3 5.5 3.7
25 15 11 10-9 6 8 10-12 13 13-25

+1.3 +1.5 -0.7 -0.3 0.0 -0.1 -0.5 +1.0 +2.5
1.2 2.0 3.2 2.8 2.5 2.6 3.0 1.5 4.0
25 12 10 9 8 10-12 15 25



116.3³25

158

4.8 58.5

+0.7	-0.1	-1.0	-0.4	0.0	-0.6	-1.2	+0.7	+1.0
4.1	4.9	5.8	5.2	4.8	5.9	6.0	4.1	3.8
25	14	12	9		7	10	11	17-25

+25

3.8 59.5

-0.3	-1.0	-0.5	0.0	-0.5	-1.1	+0.4
4.1	4.8	4.3	3.8	4.3	4.9	3.4
25	17	12	8	6	9	13-25

159

3.6 59.7

-2.6	-2.1	-1.5	-0.4	0.0	-0.2	-1.4	-1.0	+1.0
6.2	5.7	5.1	4.0	3.6	3.8	5.0	4.6	2.8
25	17	9	6	6		10-14	15-19	25

+18 \leq 12" c.l.p.
good

T.P. 10.62 117.1 12

3.5 59.8
2.75 1160.51

9' * 9' *
sec. thru pipe

-2.6	+2.0	-0.7	0.0	-0.7	-1.9	-1.2
6.1	5.5	4.2	3.5	4.2	5.9	4.7
19	10	9		9	7.4	20

160

10.1 61.0

-0.2	-1.2	-1.1	-1.5	-0.6	0.0	-0.4	-1.6	-0.9
10.3	11.3	10.7	11.6	10.7	10.1	10.5	11.7	11.0
25	19	10	9	6		8	14	16-25

161

7.7 63.4

+0.7	+0.3	-0.3	-1.2	-0.6	0.0	-0.5	-0.9	+0.1	+0.5
7.0	7.4	8.0	8.9	8.3	7.7	8.2	8.6	7.0	7.0
25	17	12	11	8		9	13	15	25

162

4.9 66.2

+0.8	+0.3	-0.4	0.0	0.0	-0.3	-0.8	+0.3	+1.2	
4.1	4.6	5.3	4.9	4.9	5.2	5.7	4.6	3.7	
25	11	9	7	3		10	14	16	25

1171 12

T.P. 1076 1179⁵ 47 2.41 1168.7

163 103 69.2

164 6.8 72.7

165 3.5 76.0

150 2.0 77.5

T.P. 519 1183.43 1.23 1178.24

166 5.4 78.0

167 5.1 78.3

168 4.6 78.8



11.6	+0.2	-0.8	-0.3	0.0	-0.2	-1.0	+0.1	+0.4	
8.7	10.1	11.1	10.6	10.3	10.5	11.3	10.2	9.9	
25	20	13	10	7	4	7	12	14	25

+1.3	-0.4	-1.8	-0.6	0.0	-0.4	-1.2	0.0
5.5	7.2	8.6	7.4	6.8	7.2	8.0	6.8
25	17	10	8	6	11	13	25

+1.0	+0.1	-1.4	-0.4	0.0	-0.3	-1.4	-0.3	+0.3
2.5	3.4	4.9	3.9	3.5	3.8	4.9	3.8	3.2
25	12	9	6	7	12	15	25	

+0.4	-1.0	-1.3	-0.3	0.0	-0.1	-1.2	-1.3	-1.2
1.6	3.0	3.3	2.3	2.0	2.1	3.2	3.3	3.2
25	12	8	5	8	12	20	25	

+0.6	-1.2	-0.4	0.0	-0.3	-1.5	-1.3	
4.8	6.6	5.8	5.4	5.7	6.9	6.7	
25	10	8	5	8	15	16	25

+0.1	-0.9	-0.7	0.0	-0.3	-1.2	
5.0	6.0	5.8	5.1	5.4	6.3	
25	16	8	8	8	13	25

+0.7	+0.3	-0.9	-0.4	0.0	-0.2	-1.2	
3.9	4.3	5.5	5.0	4.6	4.8	5.8	
25	20	16	11	8	8	12	25

1183 43

169 3.8 79.6

T.P. 5.44 1185 21 3.66 1179.77

170 4.7 80.4

171 4.7 80.5

T.P. F.G.T. Oct 30 1919 +5.85 1186 36 4.68 1180.53

172 5.90 80.5

173 4.6 81.8

174 5.6 80.7

175 8.5 77.9

176 11.4 75.0

T.P. -11.63 1174.73

+5.5 +4.53 1179.26

+5.5 4.7 74.5

✓

+0.5 -1.0 -0.6 0.0 -0.3 -1.2 -1.5
3.3 4.8 4.4 3.8 4.1 5.0 5.3
2.5 17-12 3 8 14 19-25

+0.4 -1.1 -0.3 -0.2 0.0 -0.4 -2.0 -1.0
4.4 5.5 5.6 5.0 4.8 5.2 6.8 5.8
2.5 17 6 3 8 15-20 25

+0.6 -0.9 -0.5 0.0 -0.1 -1.7 -1.3
4.1 5.6 5.4 4.7 4.8 6.4 6.0
2.5 17-8 6 7 14-20 25

-0.6 -1.4 -0.9 0.0 -0.1 -1.4 -1.4 -1.3
6.5 7.3 6.8 6.0 7.3 7.3 7.2
2.5 17 11 5.9 7 11 13 18-25

+0.4 -0.7 -0.3 -0.6 -0.1 0.0 -0.4 -1.2 -0.8
2.5 3.3 5.2 4.7 4.6 5.0 5.8 5.7
2.5 15 10 7 3 4.6 8 12 20

+1.3 +0.5 -0.7 0.0 0.0 0.0 -0.5 -0.3 -0.2
2.5 3.3 5.2 4.7 4.6 5.0 5.8 5.7
2.5 15 10 7 3 4.6 8 12 20

+2.6 +1.4 -0.6 -0.2 0.0 -0.1 -0.6 +1.8
5.9 7.1 9.1 8.7 8.6 9.1 6.7
2.0 8.25 14 16 8 5 8.5 8 12 20 +25

+1.9 +1.5 -0.1 -0.1 +0.1 0.0 +0.1 -0.7 -0.2 +1.7
2.6 9.9 11.5 11.8 11.3 11.3 12.1 11.6 10.2
2.5 19 15 10 4 11.4 7 14 16 18 21 25

→ Slice ← Good fair
12" G.I.P. [98" x 8.3" + 15" Long
Sed. thru slice:
6.4 6.8 5.2 4.8 5.1 5.8 7 7.5 + good R
2.0 10 8 4.8 5 7 9 20 15
-1.6 -2.1 -0.1 0.0 -0.3 -1.0 -2.2 2.7

1179 ³/₂₆

2

177 5.0 74.3

178 5.3 74.0

179 7.0 72.3

180 8.6 70.7

181 10.4 68.0

T.M. ok +5.16 1179.25
+3.49 1172.82

182 5.3 67.5

183 6.0 66.8

434

+34

434 6.0 66.8

184 6.0 66.8

+1.0 0.0 -0.4 -0.1 0.0 -0.4 -1.3 -2.5

4.0 5.0 5.4 5.1 5.0 5.4 6.3 2.5
2.5 2.1 1.1 7. 5.0 5. 7.2 2.5

+1.5 +0.6 -0.6 -0.1 0.0 -0.3 -1.0 -0.1
3.7 4.7 5.9 5.4 5.6 6.3 5.4
2.5 1.7 7.8 10. 7. 5.3 6. 10.7 12. 14.8 2.5

+0.4 -0.1 -0.9 -0.6 0.0 -0.3 -1.5 -1.4
6.6 7.1 7.9 7.6 7.0 7.3 8.5 8.6
2.5 1.8 10. 6. 7.0 8. 13. 2.0 + 2.5

+1.6 +0.6 -1.5 -0.8 0.0 -0.2 -1.1 -0.6 -0.4
7.0 8.0 10.1 9.4 8.7 8.7 9.7 9.2 2.0
2.5 1.4 9. 6. 8.6 8. 13. 14. 2.5

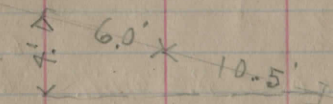
+0.8 +0.1 -0.5 -1.0 -0.6 0.0 -0.3 -0.8 +0.4 +0.2
9.6 10.3 10.9 11.4 11.0 10.7 11.2 10.0 9.8
2.5 1.9 7. 7. 5. 10.4 8. 11.8 13. 17. 22.8 2.5

+1.0 -0.4 -0.9 0.0 -0.2 -0.7 0.0

4.3 5.7 6.2 5.3 5.3 6.0 5.3 2.5
2.5 9. 5. 5.3 9. 1.9 1.8 2.5

+0.3 -0.7 0.0 -0.2 -0.9 -1.4
5.7 6.7 6.2 6.9 7.7
2.5 7.2 6.0 7. 12. 2.5

12" C.I.R. Slice cond. good



Section thru slice

-1.0 -1.6 -2.2 -0.7 0.0 -0.6 -2.5 -3.4
7.0 7.6 8.2 6.7 6.0 6.6 8.5 9.7
15. 10. 7. 6. 6.0 7. 11.4 20. 35.

+1.7 +1.1 -0.8 -0.1 0.0 -0.1 -0.5 +0.4 +0.8
4.3 4.9 6.7 6.1 6.1 6.5 5.6 5.2
2.5 1.4 8.8 11. 3. 6.0 7. 13. 19. 25.

Rain

185 1172.82 4.8 68.0

186 6.5 66.3

187 9.3 64.5

+89

+89

188

+45

TP

+7.53 1172.76

B.M.

6.56

-6.57

100' J. D. & Gill 6.2 66.6

200' " " " 6.7 66.1

100' " N. & " 7.1 65.7

200' " " " 6.0 66.8

100' E. & Center Rd. 7.7 68.1

200' " " " 4.0 68.8

+1.0 +0.5 -0.4 -0.4 0.0 +0.3 0.0 -0.2 +0.3

3.7 4.3 5.4 5.4 4.5 4.8 5.1 4.5
23825 7.0 8.8 7. 4.8 6. 7.0 7.5 2.5

+1.4 +1.7 +0.8 -0.4 0.0 +0.4 +0.3 -0.1 0.0
5.1 4.8 5.7 7.1 5.9 6.2 6.6 6.5
25. 20. 11. 6. 6.5 7.0 7.2 16. 25

+3.2 +2.0 -0.5 0.0 +0.5 -0.1 -0.9 +0.4
5.1 5.7 8.7 9.3 7.8 8.4 9.2 7.7
25. 15. 4.8 7. 7.0 16. 17. 25

Stone Box Culvert 2 1/2 x 3' x 25'
Condition Good - S.W. Parapet on the ground

Par. 2' x 2' x 6' 12.6' x 3' x 22'

2.8 Top of Parapet 11.0
2.8 Top of Stone 11.7
-0.9
11.0 Parapet 11.3
4. 3. 7.2 7.0 2.1 11.7
2.8 3. 7.2 7.0 2.1 11.7

-0.9 -1.2 -0.1 0.0 +0.8 +0.6 -0.8 -3.3
2.8 2.3 2.2 8.1 7.3 7.8 8.7 11.7
25. 3. 2. 8.1 11. 16. 22. 25

-1.2 -0.1 +0.2 0.0 +0.1 -0.4 -1.2 -3.4
2.5 7.7 7.1 7.2 7.7 8.5 10.7
35. 25. 19. 9.3 14. 25. 30. 35

Side Culvert + 8 + 10
O.K.

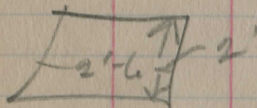
3 + 75

14' CI 28' Long

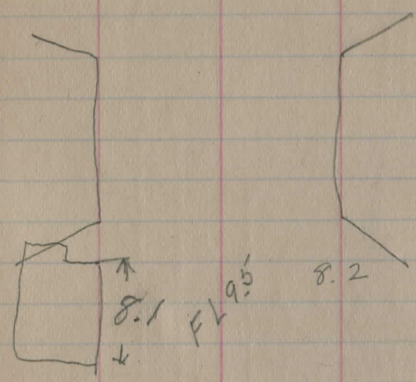
25' st
+ 8' \neq

Cul 1 + 10

40' Long, $\leftarrow 7' \rightarrow$



Bridge 136 + 35



PAGE 58 WAS
MISSNG FROM THE BOOK

Elev. Bridge 127+50

West Abut 1018.22

East Abut 1016.86

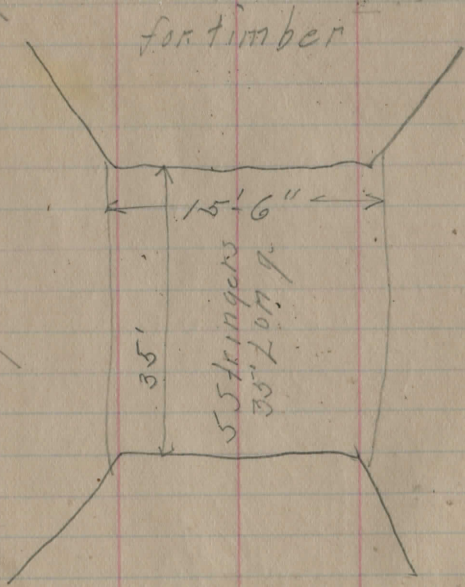
1016.70 B.M.
6.59

1018.29

1018.29

1016.86
1.43

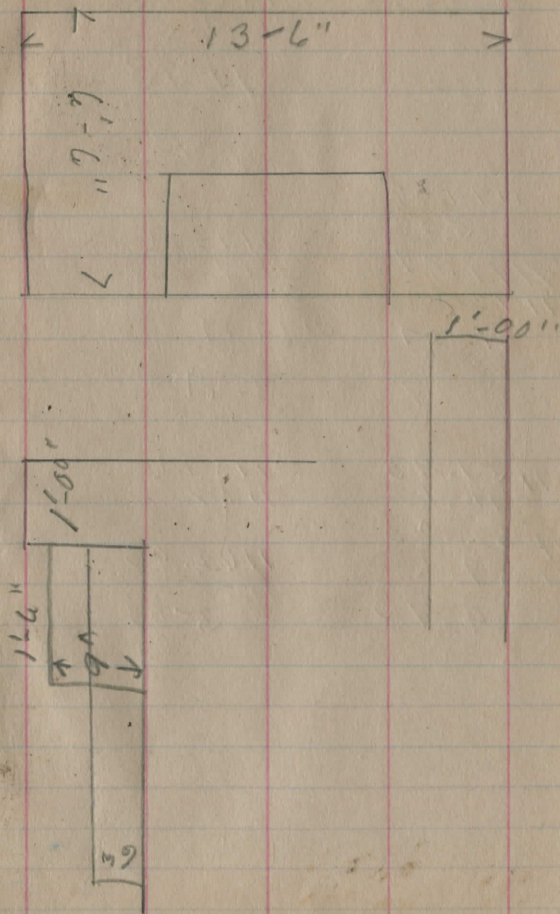
34' by 15'-6" Bridge Flooring
 10 10
 009.75



35-
 175-

155-
 34
 620
 455
 822.

1011.70
 5.30
 1017.00
 1010
 7.00
 4.55



1174.09
2.34

1176.43
11.65
11.43

1174.09
5.78
1179.87
1172.6
7.27
1.50
5.77

1151.43
10.6
1162.03
1157.6
4.43

1165
1164.5

1176.43
11.65
11.93
5
11.43

1172.6
1172.2
1179.87
1172.2
7.67

1157.6
1158
1162.03
1158
5.03
3.03

ER

Bainbridge at X roads, in E. cutv.
 w. side of road; aluminum tablet
 stamped 1166 Adj. 1903 Elev = 1,166.180 Ft.

Sta 0+0. = 1090.38
 B.M. 42' Made. Spike Elev = 1098.64

Chillicothe Rd
 Whil. in notch of Elm Rt.
 Elev = 1206.52

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
 DRAWING MATERIALS AND SURVEYING INSTRUMENTS

PLEASE RETURN TO
 GAUGA COUNTY ENGINEER

COURT HOUSE

CHARDON, O.

PHONE BOX

Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.
1	.0000	1	.0000	1	.0000	1	.0000	1	.0000	1	.0000	1	.0000	1	.0000
2	.0001	2	.0002	2	.0004	2	.0008	2	.0016	2	.0032	2	.0064	2	.0128
3	.0003	3	.0006	3	.0009	3	.0018	3	.0036	3	.0072	3	.0144	3	.0288
4	.0004	4	.0008	4	.0012	4	.0024	4	.0048	4	.0096	4	.0192	4	.0384
5	.0005	5	.0010	5	.0015	5	.0030	5	.0060	5	.0120	5	.0240	5	.0480
6	.0006	6	.0012	6	.0018	6	.0036	6	.0072	6	.0144	6	.0288	6	.0576
7	.0007	7	.0014	7	.0021	7	.0042	7	.0084	7	.0168	7	.0336	7	.0672
8	.0008	8	.0016	8	.0024	8	.0048	8	.0096	8	.0192	8	.0384	8	.0768
9	.0009	9	.0018	9	.0027	9	.0054	9	.0108	9	.0216	9	.0432	9	.0864
10	.0010	10	.0020	10	.0030	10	.0060	10	.0120	10	.0240	10	.0480	10	.0960
11	.0011	11	.0022	11	.0033	11	.0066	11	.0132	11	.0264	11	.0528	11	.1056
12	.0012	12	.0024	12	.0036	12	.0072	12	.0144	12	.0288	12	.0576	12	.1152
13	.0013	13	.0026	13	.0039	13	.0078	13	.0156	13	.0312	13	.0624	13	.1248
14	.0014	14	.0028	14	.0042	14	.0084	14	.0168	14	.0336	14	.0672	14	.1344
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16	.0016	16	.0032	16	.0048	16	.0096	16	.0192	16	.0384	16	.0768	16	.1536
17	.0017	17	.0034	17	.0051	17	.0102	17	.0204	17	.0408	17	.0816	17	.1632
18	.0018	18	.0036	18	.0054	18	.0108	18	.0216	18	.0432	18	.0864	18	.1728
19	.0019	19	.0038	19	.0057	19	.0114	19	.0228	19	.0456	19	.0912	19	.1824
20	.0020	20	.0040	20	.0060	20	.0120	20	.0240	20	.0480	20	.0960	20	.1920
21	.0021	21	.0042	21	.0063	21	.0126	21	.0252	21	.0504	21	.1008	21	.2016
22	.0022	22	.0044	22	.0066	22	.0132	22	.0264	22	.0528	22	.1056	22	.2112
23	.0023	23	.0046	23	.0069	23	.0138	23	.0276	23	.0552	23	.1104	23	.2208
24	.0024	24	.0048	24	.0072	24	.0144	24	.0288	24	.0576	24	.1152	24	.2304
25	.0025	25	.0050	25	.0075	25	.0150	25	.0300	25	.0600	25	.1200	25	.2400
26	.0026	26	.0052	26	.0078	26	.0156	26	.0312	26	.0624	26	.1248	26	.2496
27	.0027	27	.0054	27	.0081	27	.0162	27	.0324	27	.0648	27	.1296	27	.2592
28	.0028	28	.0056	28	.0084	28	.0168	28	.0336	28	.0672	28	.1344	28	.2688
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32	.0032	32	.0064	32	.0096	32	.0192	32	.0384	32	.0768	32	.1536	32	.3072
33	.0033	33	.0066	33	.0099	33	.0198	33	.0396	33	.0792	33	.1584	33	.3168
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35	.0035	35	.0070	35	.0105	35	.0210	35	.0420	35	.0840	35	.1680	35	.3360
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52	.0052	52	.0104	52	.0156	52	.0312	52	.0624	52	.1248	52	.2496	52	.4992
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56	.0056	56	.0112	56	.0168	56	.0336	56	.0672	56	.1344	56	.2688	56	.5376
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